



# CFD analysis of delayed ignition hydrogen releases from a train inside a tunnel

---

[Tolias I.C.](#)<sup>1</sup>, [Rattigan W.](#)<sup>2</sup>, [Lyons K.](#)<sup>2</sup>, [Koumroglou V.C.](#)<sup>3</sup>, [Venetsanos A.G.](#)<sup>1</sup>


<sup>1</sup>*Environmental Research Laboratory, **National Centre for Scientific Research Demokritos**, Agia Paraskevi, Athens, 15341, Greece*

<sup>2</sup>**HSE Science and Research Centre**, Buxton, United Kingdom

<sup>3</sup>Core department, **National and Kapodistrian University of Athens**, Euripus Campus, Greece

[tolias@ipta.demokritos.gr](mailto:tolias@ipta.demokritos.gr)



- Hydrogen
  - Significant reductions in greenhouse gas emissions
  - Significant improvements in energy efficiency
- Accidental release in confined space → catastrophic consequences in the case of an explosion
- Computational Fluid Dynamics (CFD)
  - Attractive methodology for risk assessment: Accurate modelling of the geometry and the flow
- HyTunnel project<sup>1</sup> 
  - The aim was perform pre-normative research for safety of hydrogen driven vehicles and transport through tunnels and similar confined spaces

<sup>1</sup><https://hytunnel.net/>



- Delayed ignition experiments that were recently performed by HSE in a model of a tunnel were simulated using CFD
  - Hydrogen release and dispersion
  - Delayed ignition (deflagration)
  
- The **aims of the work** are:
  - analyze the experiments using CFD models to gain a deeper understanding of the phenomena
  - investigate the impact of certain parameters, such as wind and ignition delay, on the results.
  - to verify the accuracy of our CFD model



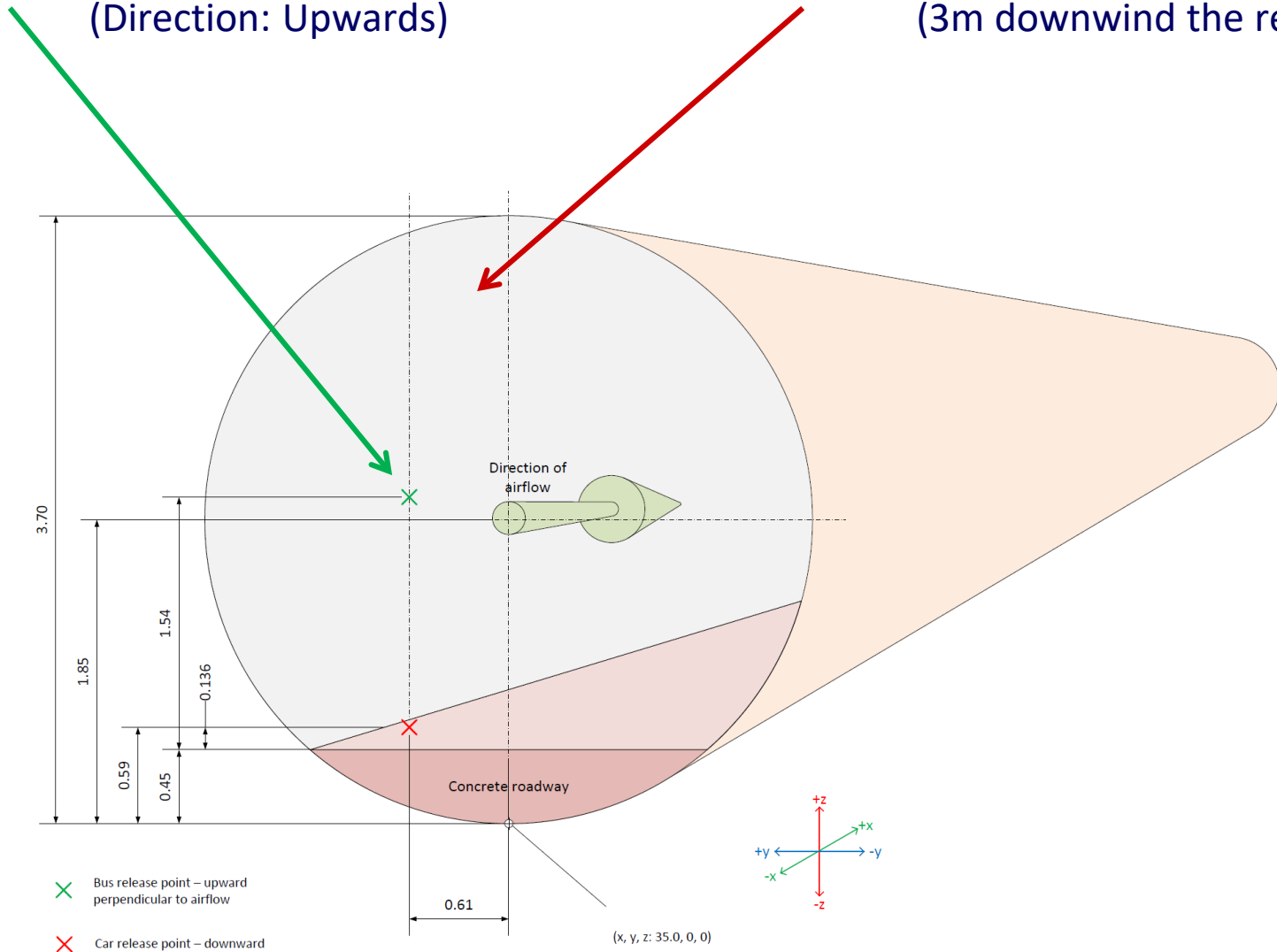
- Geometry:
  - Tunnel length: 70 m
  - Maximum height: 3.25 m
  - Horseshoe cross section
  - Case without congestion
- Forced or natural ventilation





■ **Release:**  $x=35, y=0.6, z=1.54$  m  
(Direction: Upwards)

**Ignition:**  $x=38, y=0.6, z=2.95$  m  
(3m downwind the release)





## ■ Basic examined cases in this work

- Test 6: Only hydrogen concentrations are measured
- Test 25: Ignited case, overpressure measurements

Test Number	Ignited	Ignition delay	Congestion	Wind type	Wind range
6	No	–	No	Forced ventilation	0.8 – 1.5
25	Yes	8.5 s	No	Forced ventilation	1.0 – 1.6

## ■ Secondary cases

- Tests 55-57: Ignition delay effect

Test Number	Ignited	Ignition delay	Congestion	Wind type	Wind range
55	Yes	0.0 s	No	<b>Natural</b> ventilation	1.5 – 1.9*
56	Yes	1.8 s	No	<b>Natural</b> ventilation	1.5 – 1.9*
57	Yes	6.5 s	No	<b>Natural</b> ventilation	1.5 – 1.9*

\*Great uncertainty of the wind speed

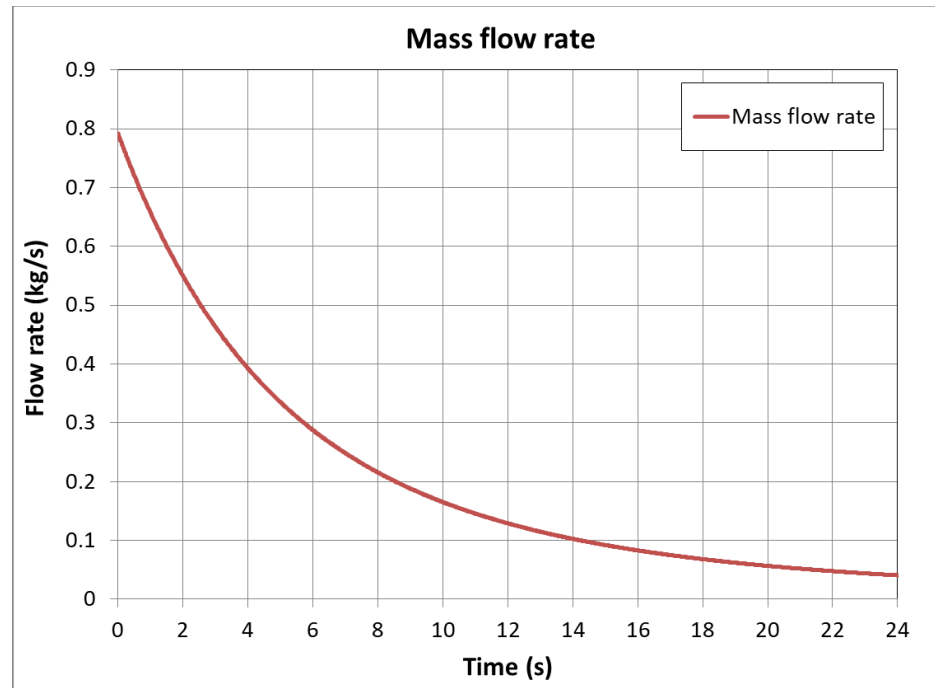


## ■ Hydrogen

- Train release case
- Storage mass: 5.55 kg
- Storage pressure: 580 bars

## ■ Release

- Pressure inside the tank was used to estimate mass flow rate





## ■ CFD modelling

- ADREA-HF code
- Continuity, Navier-Stokes, Energy, Species mass fraction equations
- Turbulence: k-ε model (Kato, Launder 1993 modification)

## ■ Deflagration model:

- Turbulent burning velocity model<sup>1</sup>

$$S_T = \Xi_k \cdot \Xi_{lp} \cdot \left[ S_L + u' \left( 1 + Da^{-2} \right)^{-1/4} \right]$$

Turbulence that is generated by the flame front itself

non-equidiffusive effects

Turbulence that exists in front of the flame front (Schmid's relation)

<sup>1</sup>Tolias I.C., Venetsanos A.G., 2018, An improved CFD model for vented deflagration simulations – Analysis of a medium-scale hydrogen experiment, IJHE, 43 (52), 23568-84





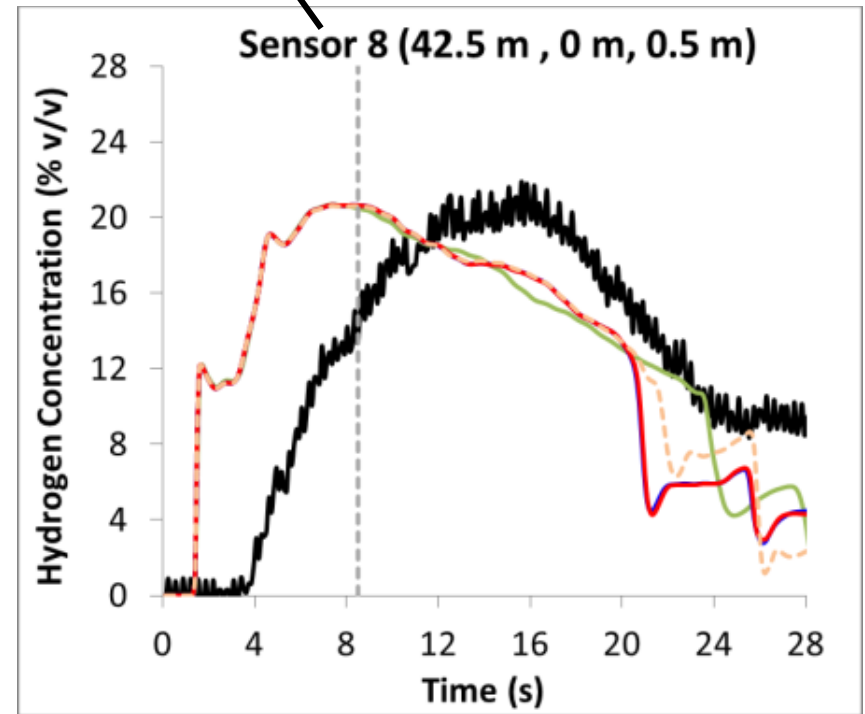
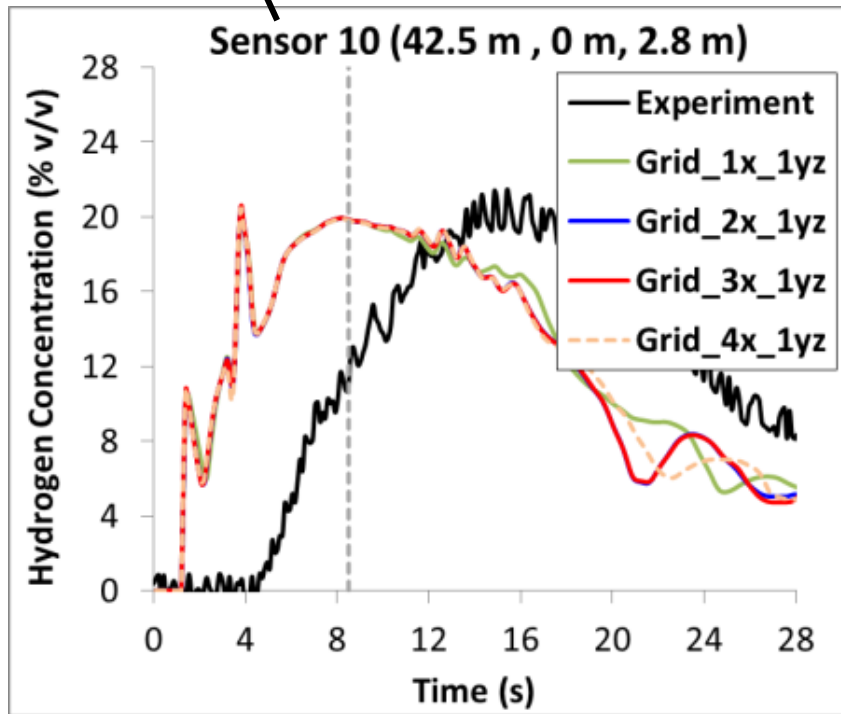
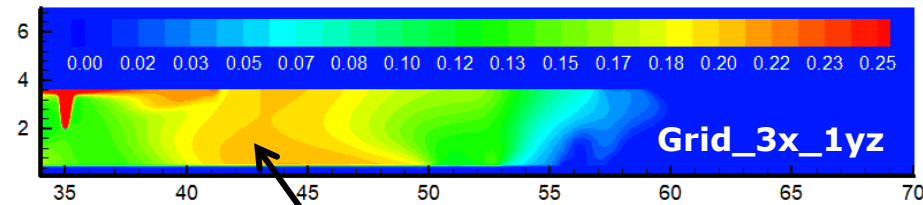
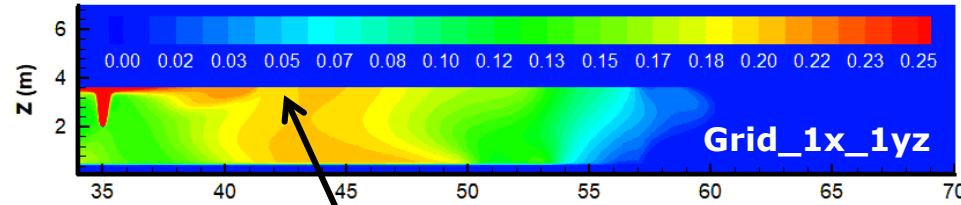
## ■ Grid sensitivity study

- First the grid sensitivity study in the x direction was examined
- Four different grids were used
- Wind speed equal to 1.3 m/s is used (average of the experimental measurements)

Grid cases						
ID	Name	Number of cells in x direction	Number of cells in y direction	Number of cells in z direction	Total number of active cells	Number of cells in source
1	Grid_1x_1yz	<b>288</b>	117	94	1,242,886	4
2	Grid_2x_1yz	<b>490</b>	117	94	1,821,909	4
3	Grid_3x_1yz	<b>646</b>	117	94	2,268,849	4
4	Grid_4x_1yz	<b>788</b>	117	94	2,679,705	4

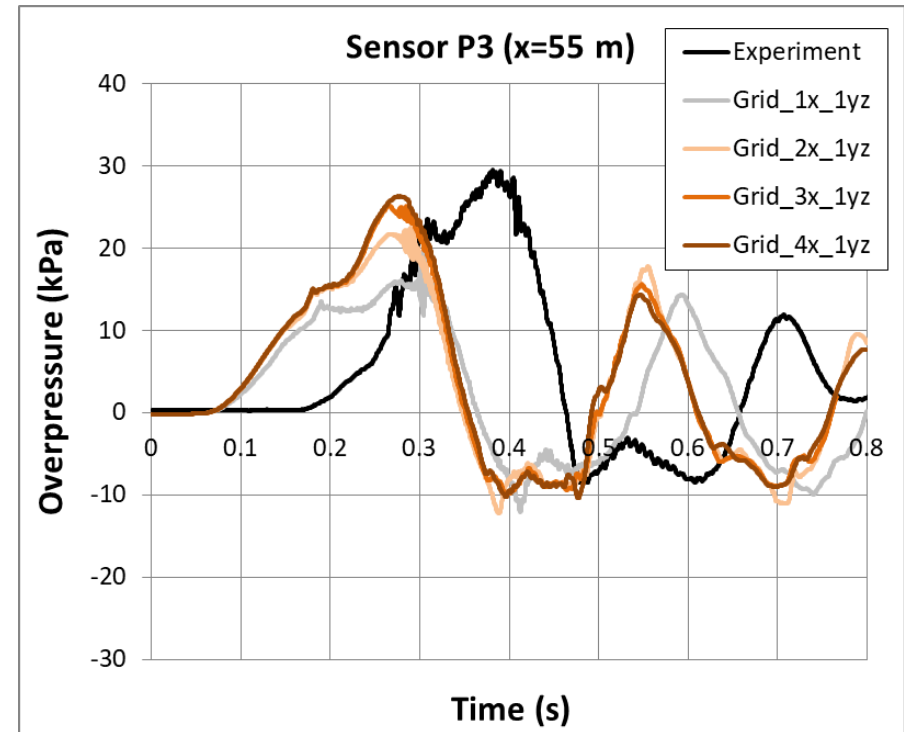
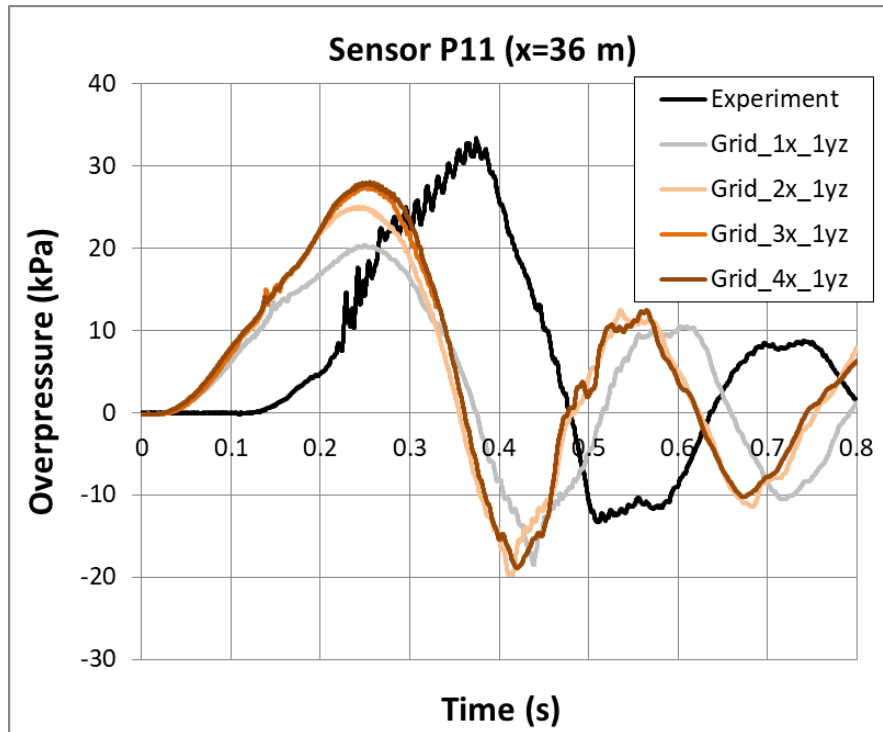


- **Grid sensitivity study: x direction**
  - Hydrogen concentrations at ignition time (8.5 s)





- **Grid sensitivity study: x direction**
  - Overpressures (ignition at x=38 m)



- Grid independency is achieved in 3<sup>rd</sup> grid

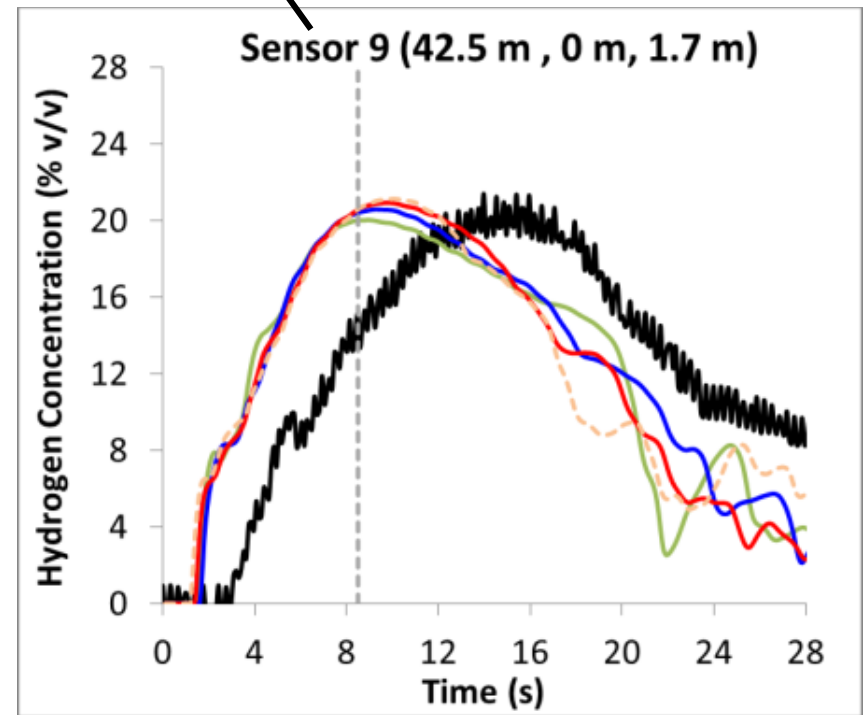
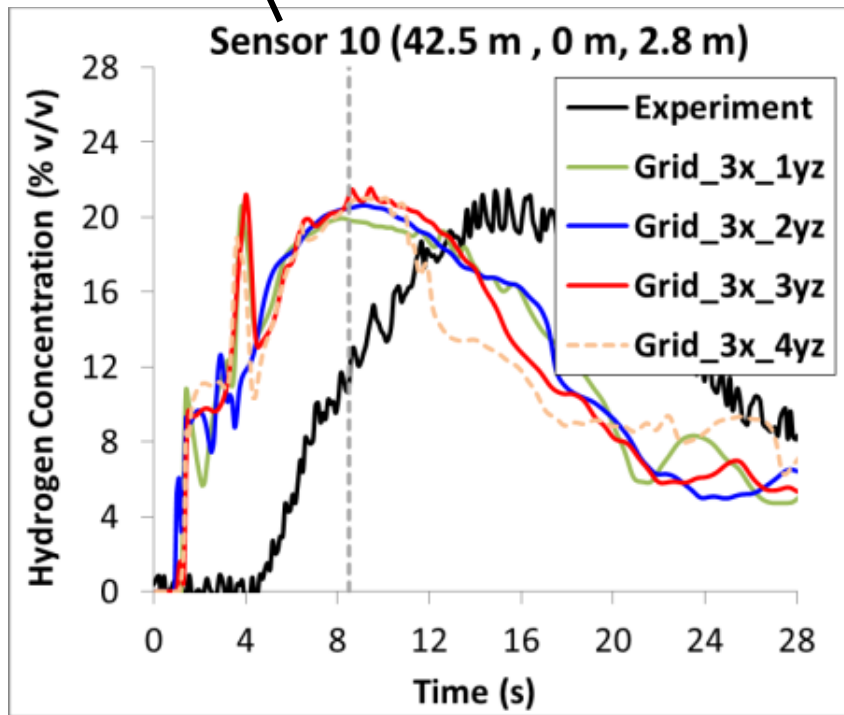
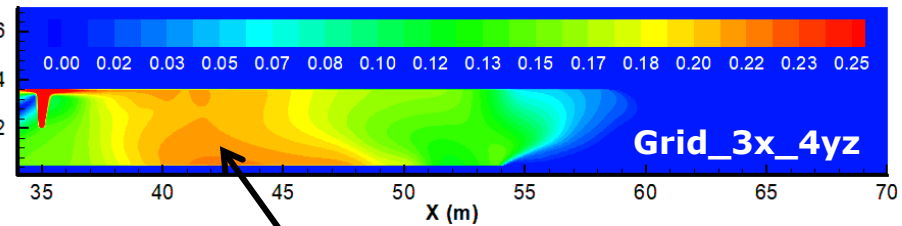
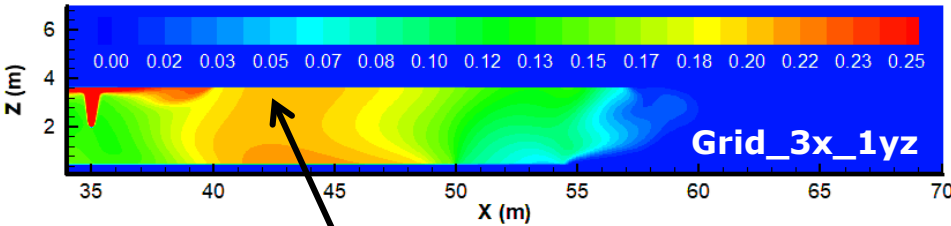


- **Grid sensitivity study**
  - y and z direction was examined
  - Four different grids were used

Grid cases						
ID	Name	Number of cells in x direction	Number of cells in y direction	Number of cells in z direction	Total number of active cells	Number of cells in source
3	Grid_3x_1yz	646	117	94	2,268,849	4
5	Grid_3x_2yz	646	<b>144</b>	<b>114</b>	3,804,269	4
6	Grid_3x_3yz	646	<b>152</b>	<b>124</b>	4,470,576	4
7	Grid_3x_4yz	<b>658</b>	<b>171</b>	<b>142</b>	6,384,087	<b>9</b>

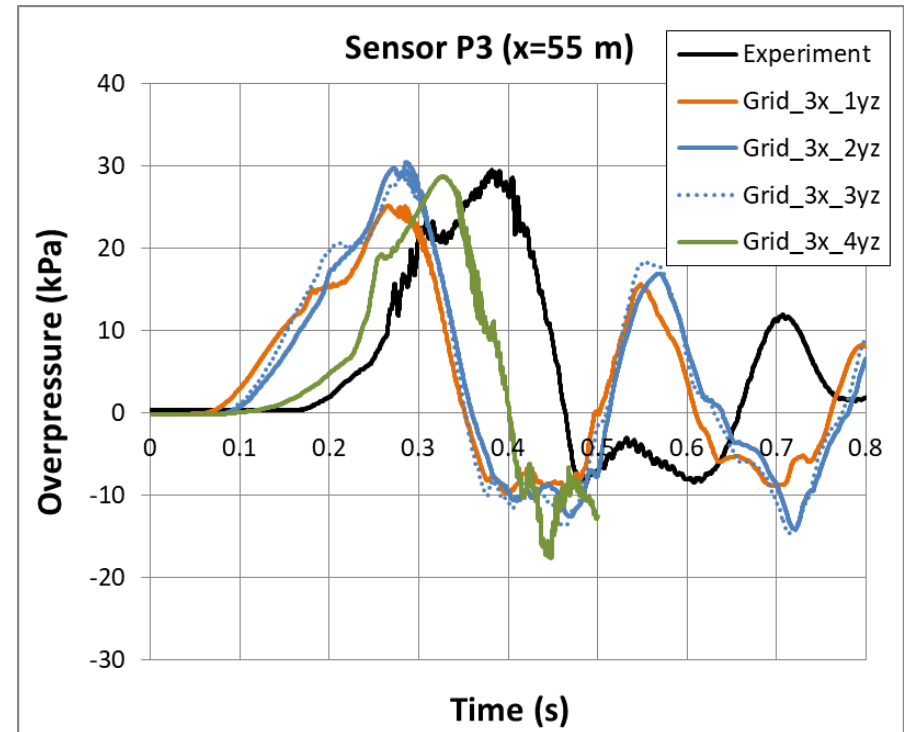
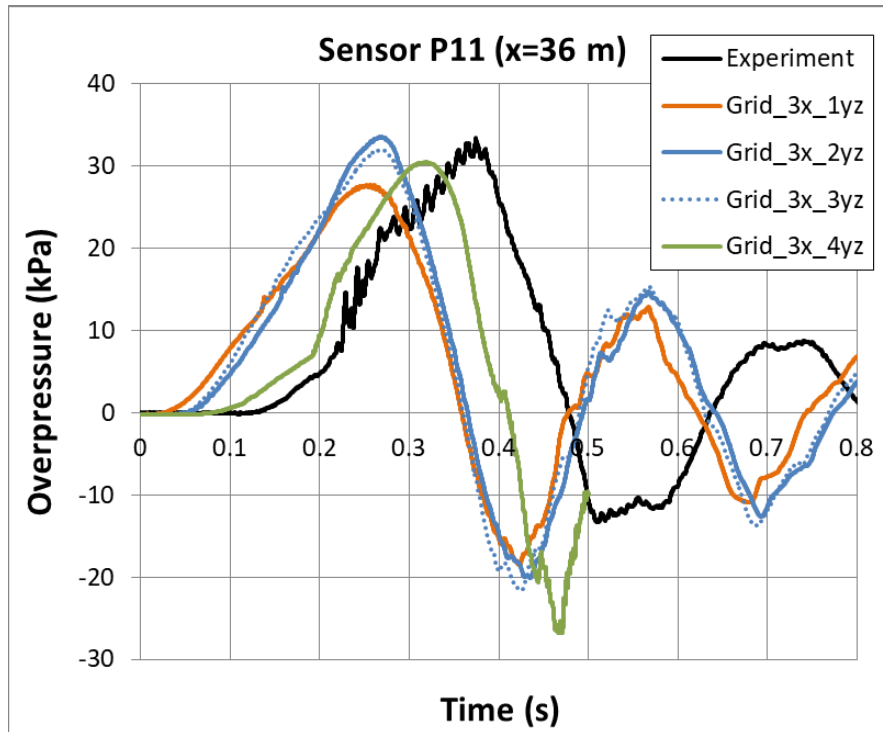


- **Grid sensitivity study: y, z direction**
  - Hydrogen concentrations at ignition time (8.5 s)





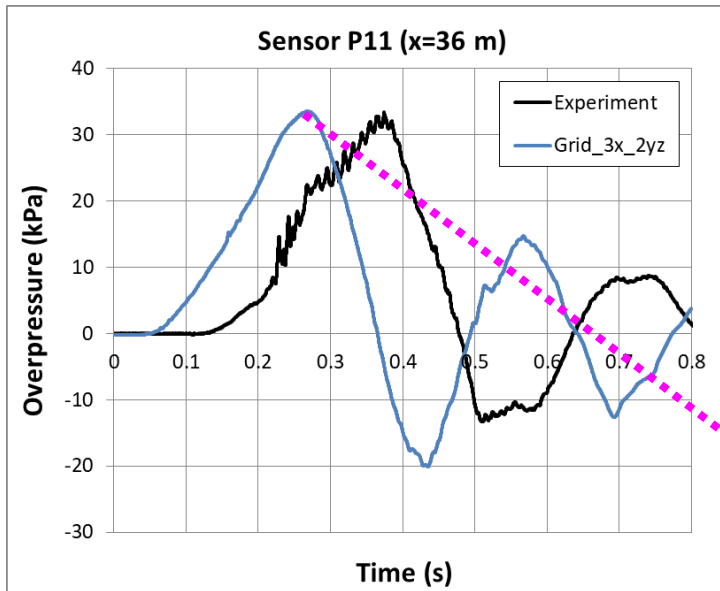
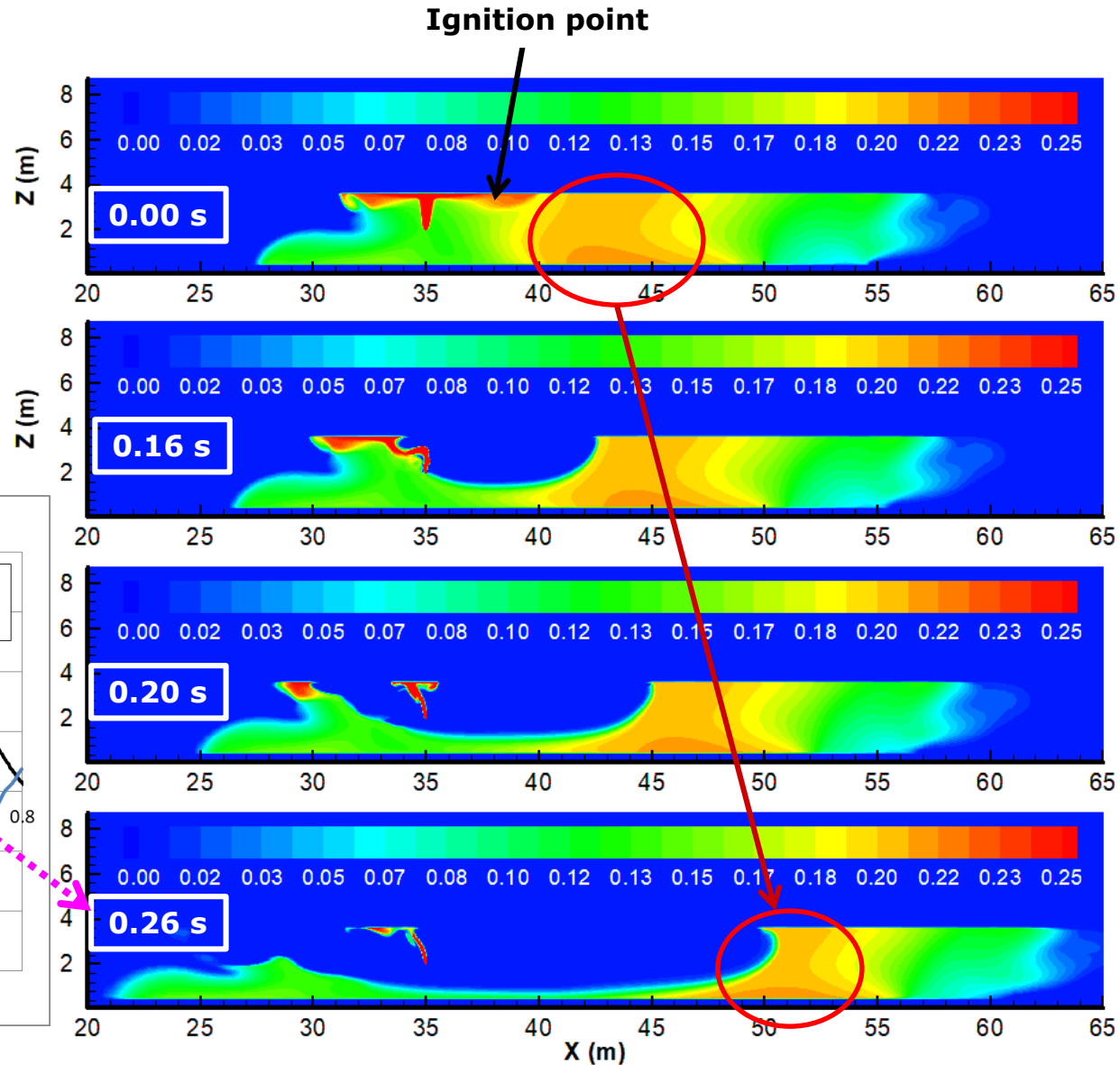
- **Grid sensitivity study: y, z direction**
  - Overpressures (ignition at x=38 m)



- The second grid (blue line) is used in the rest of the study

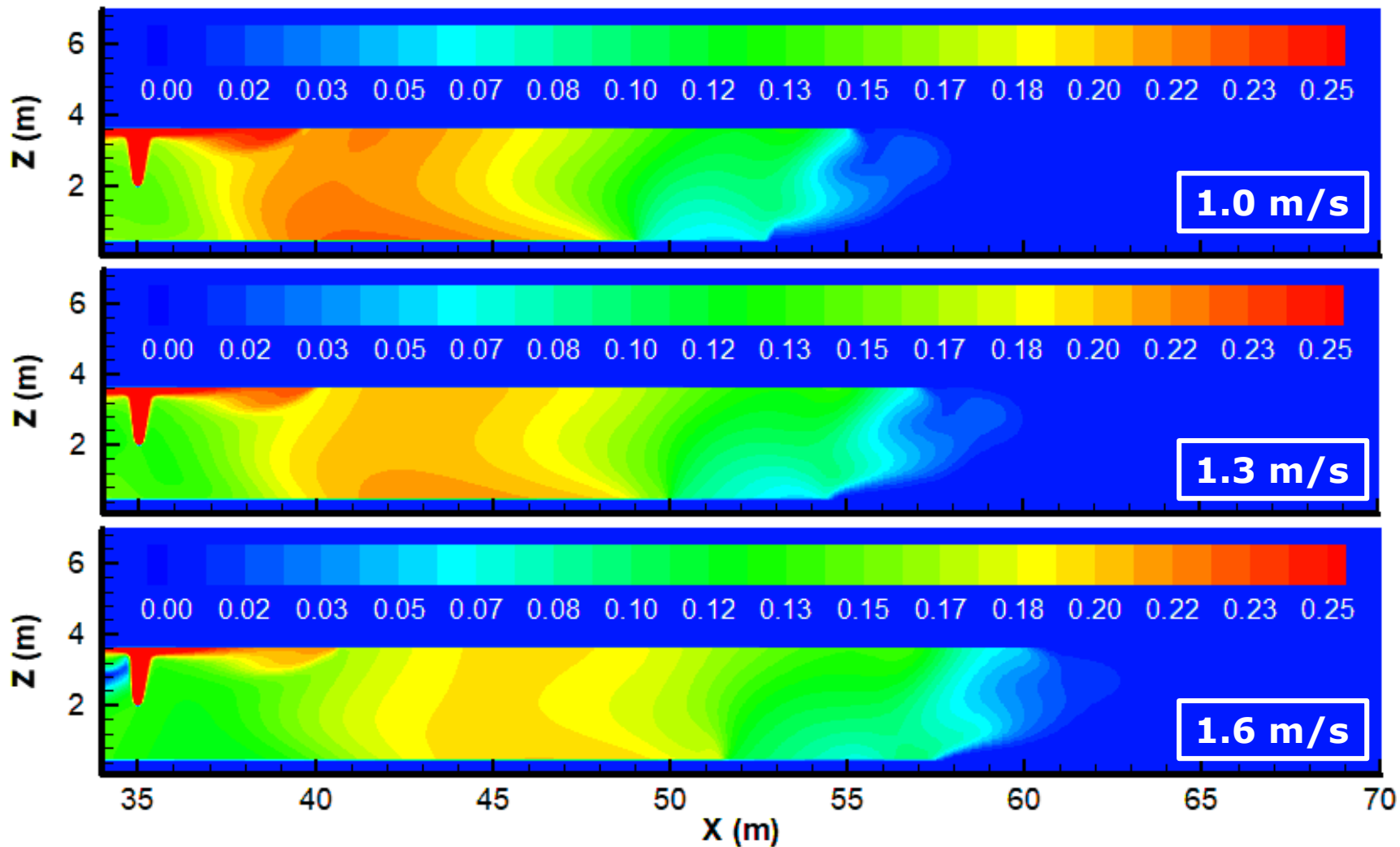


## Flame propagation





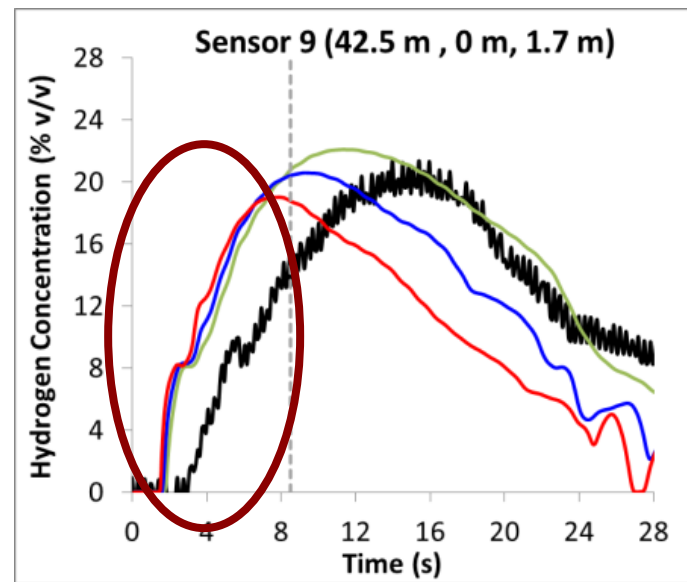
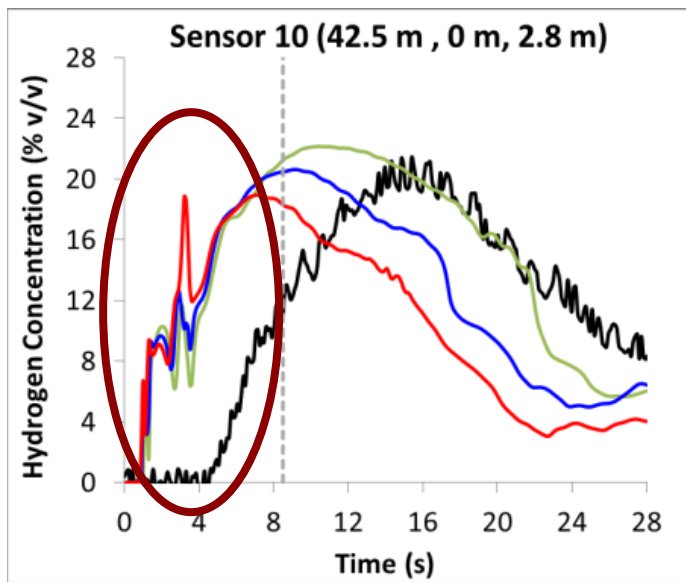
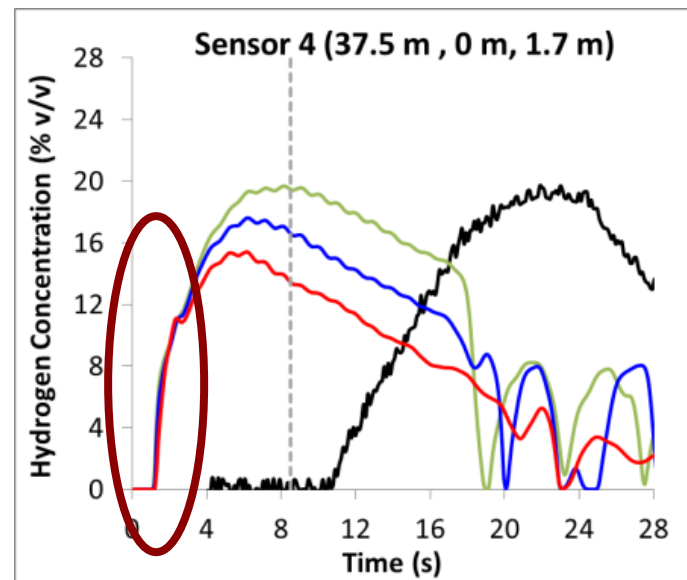
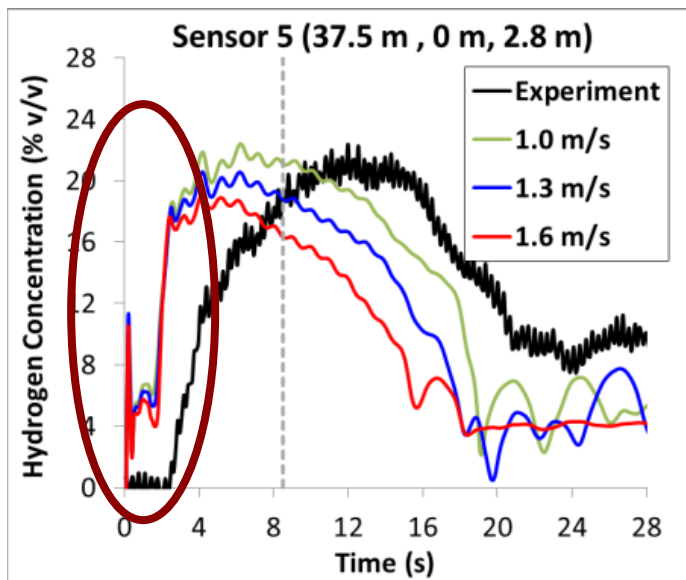
- Three wind velocities were examined





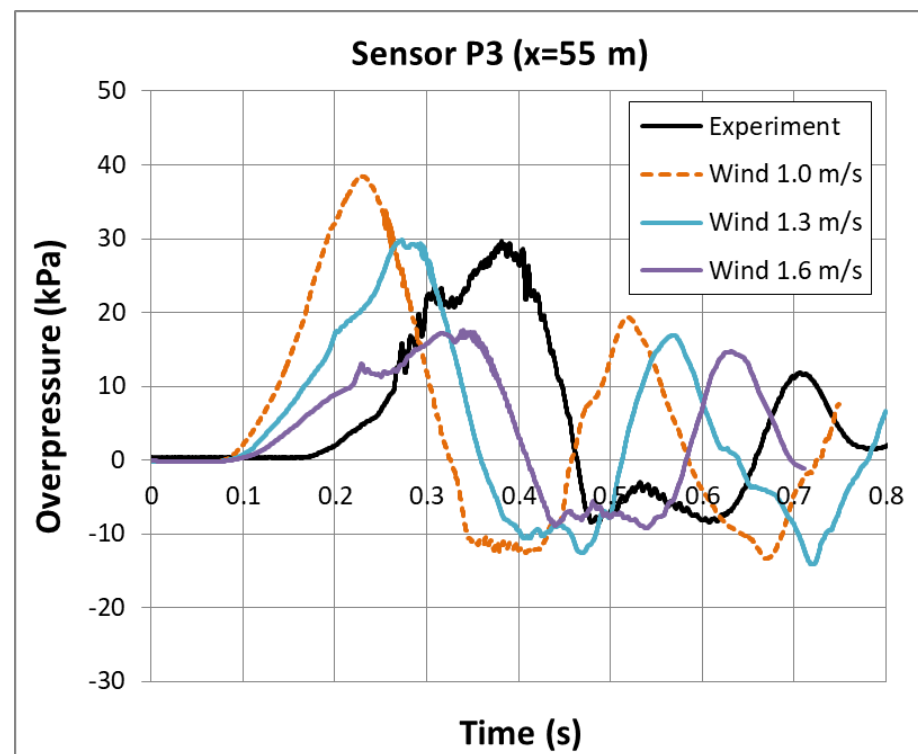
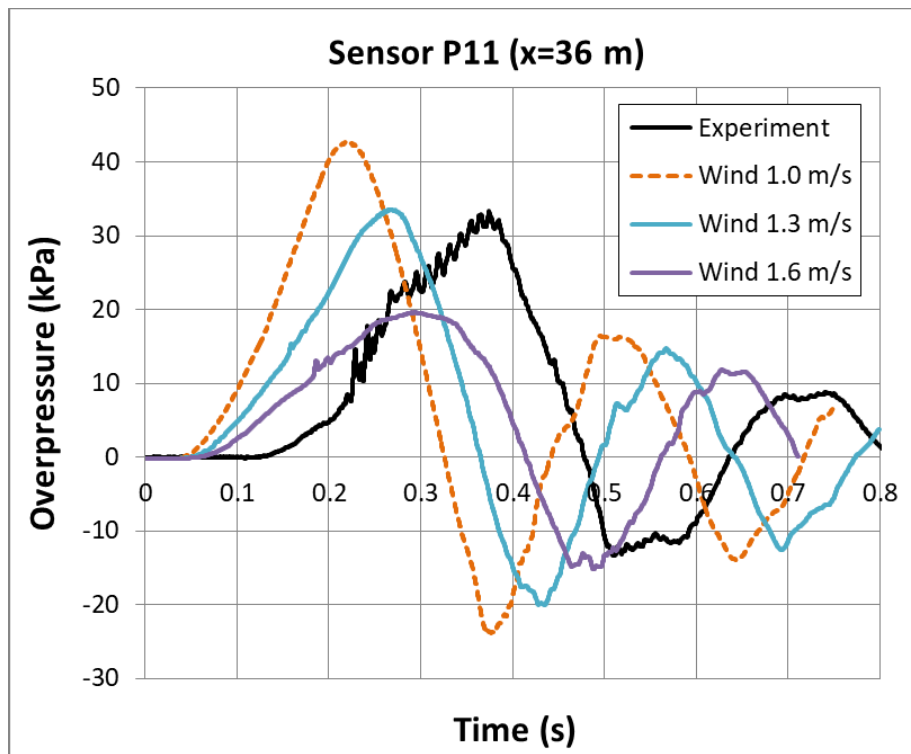


# CFD results – Wind effect





## Overpressures



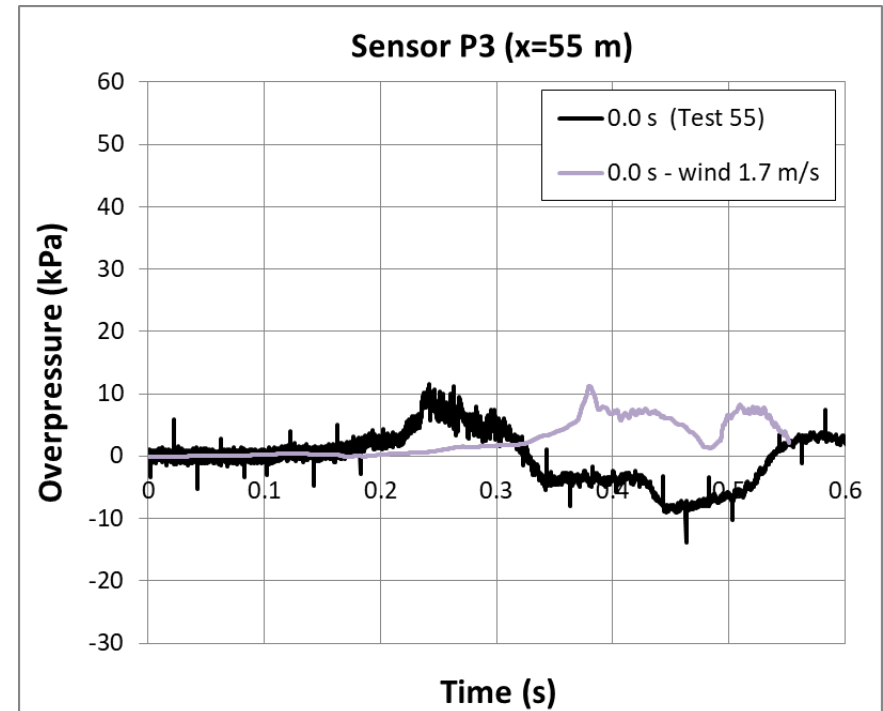
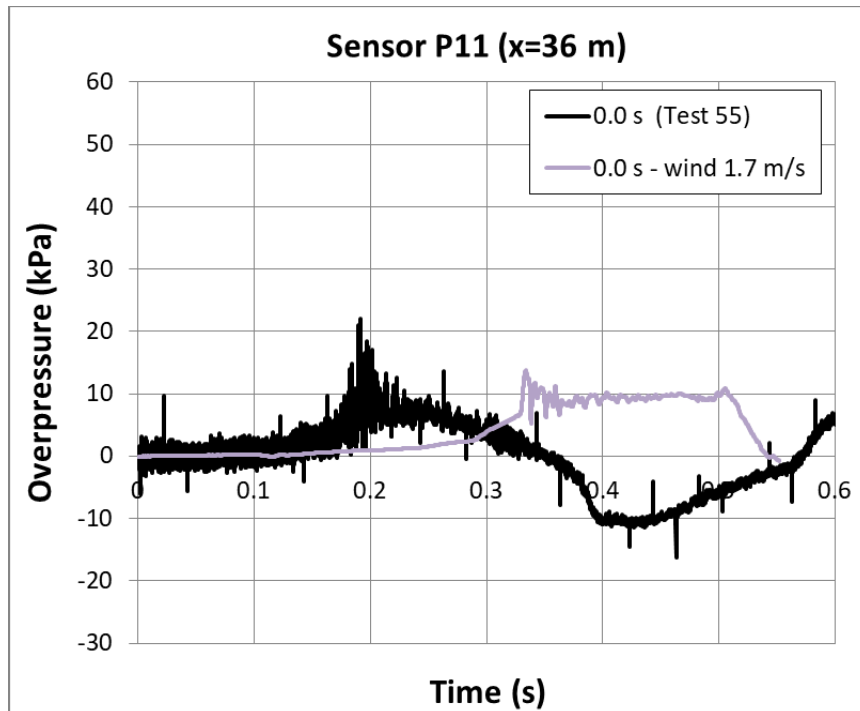
- 1.3 m/s to 1.6 m/s: 23% increase of wind results in 65% decrease in overpressure



- Simulations of other tests: Ignition delay
  - Tests 55-57: Ignition delay effect

Test Number	Ignited	Ignition delay	Congestion	Wind type	Wind range
55	Yes	0.0 s	No	Natural ventilation	1.5 – 1.9*
56	Yes	1.8 s	No	Natural ventilation	1.5 – 1.9*
57	Yes	6.5 s	No	Natural ventilation	1.5 – 1.9*

\*Great uncertainty of the wind speed



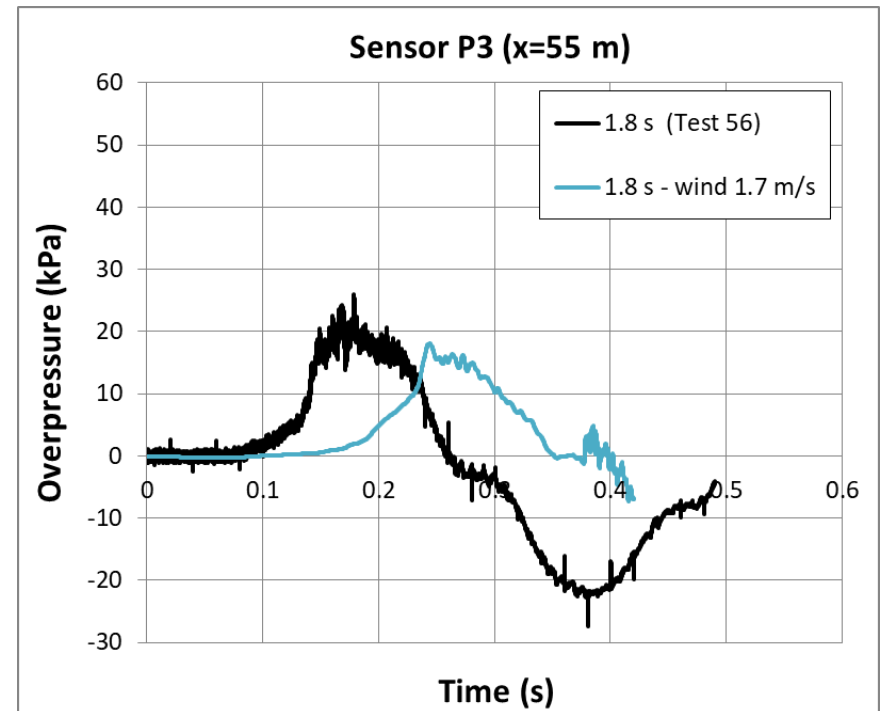
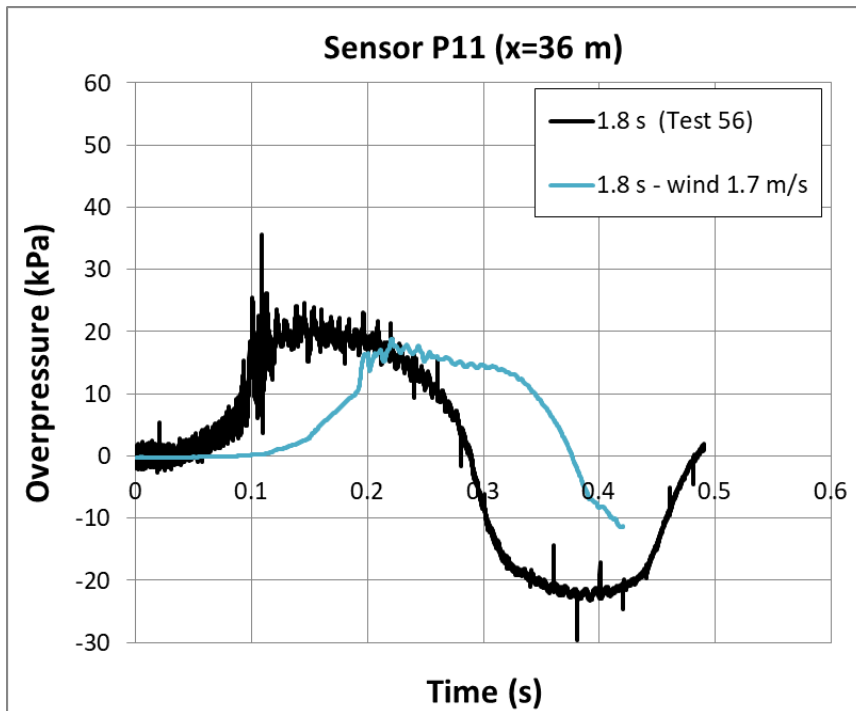


# CFD results – Ignition delay

- Simulations of other tests: Ignition delay
  - Tests 55-57: Ignition delay effect

Test Number	Ignited	Ignition delay	Congestion	Wind type	Wind range
55	Yes	0.0 s	No	Natural ventilation	1.5 – 1.9*
56	Yes	1.8 s	No	Natural ventilation	1.5 – 1.9*
57	Yes	6.5 s	No	Natural ventilation	1.5 – 1.9*

\*Great uncertainty of the wind speed

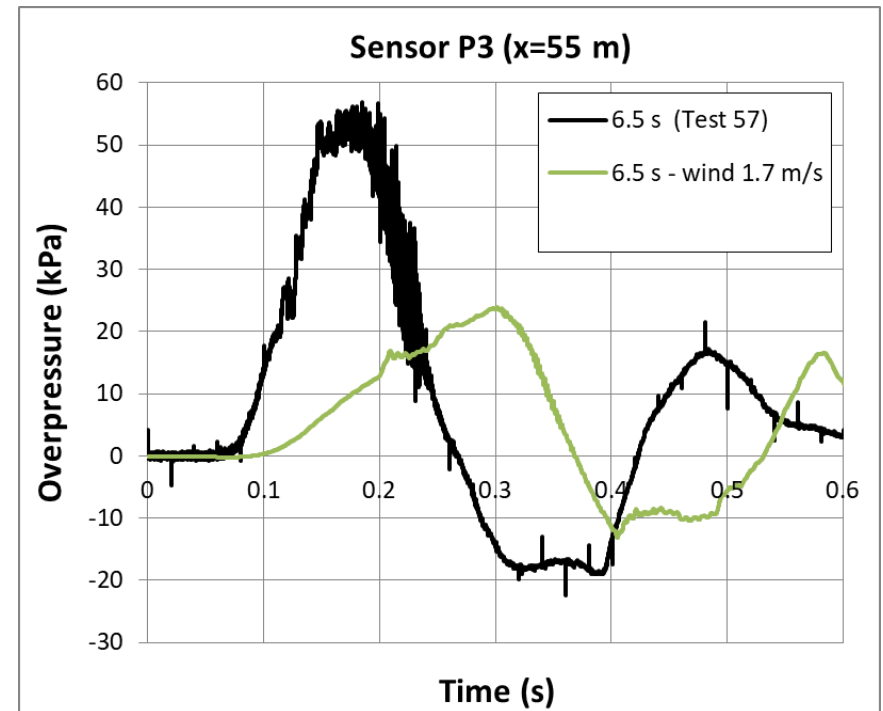
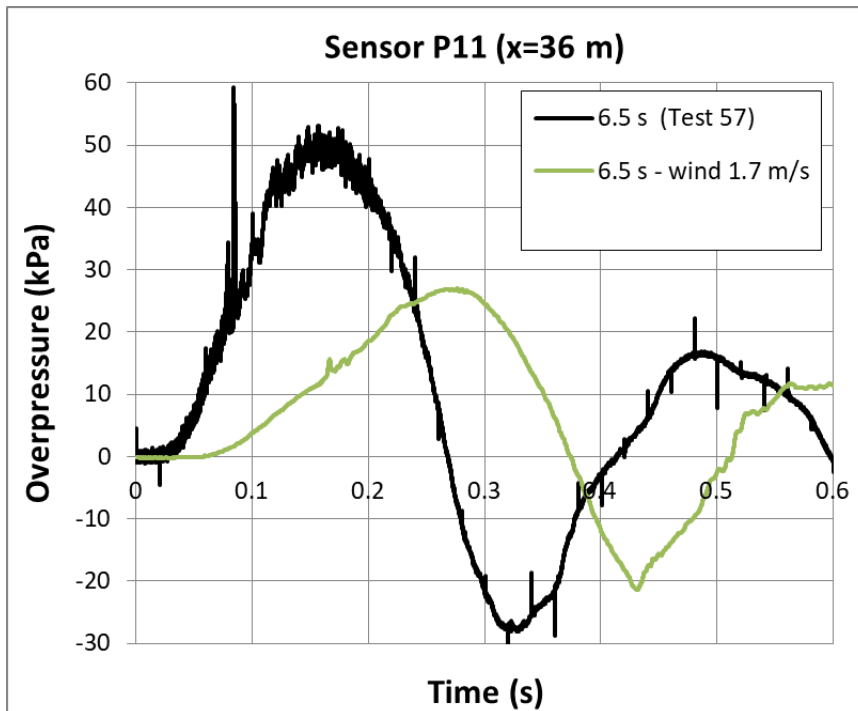




- Simulations of other tests: Ignition delay
  - Tests 55-57: Ignition delay effect

Test Number	Ignited	Ignition delay	Congestion	Wind type	Wind range
55	Yes	0.0 s	No	Natural ventilation	1.5 – 1.9*
56	Yes	1.8 s	No	Natural ventilation	1.5 – 1.9*
57	Yes	6.5 s	No	Natural ventilation	1.5 – 1.9*

\*Great uncertainty of the wind speed



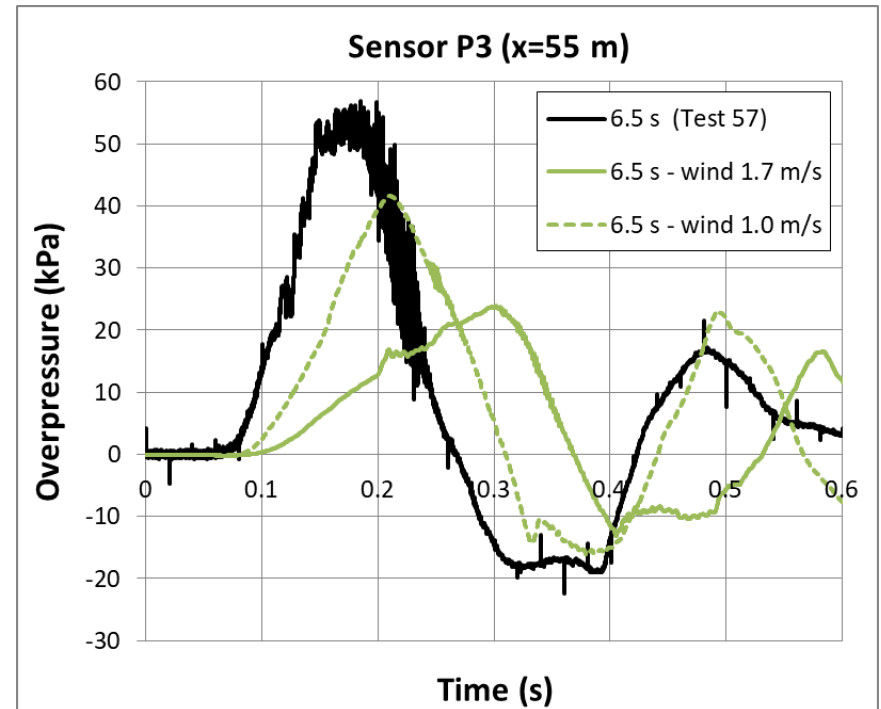
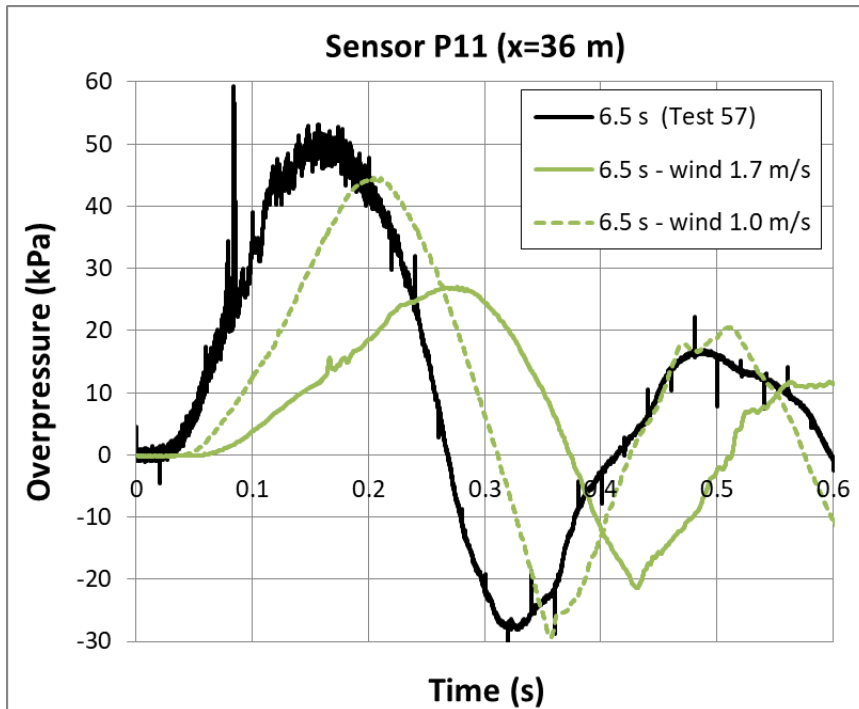


# CFD results – Ignition delay

- Simulations of other tests: Ignition delay
  - Tests 55-57: Ignition delay effect

Test Number	Ignited	Ignition delay	Congestion	Wind type	Wind range
55	Yes	0.0 s	No	Natural ventilation	1.5 – 1.9*
56	Yes	1.8 s	No	Natural ventilation	1.5 – 1.9*
57	Yes	6.5 s	No	Natural ventilation	1.5 – 1.9*

\*Great uncertainty of the wind speed

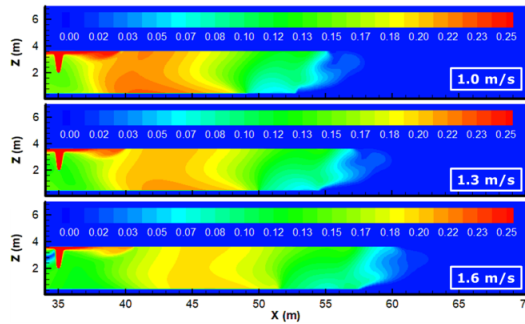
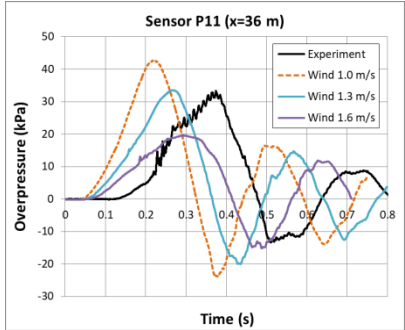
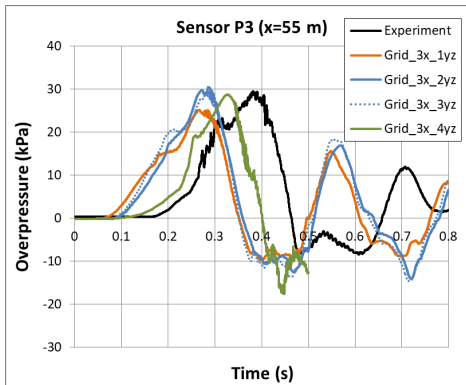




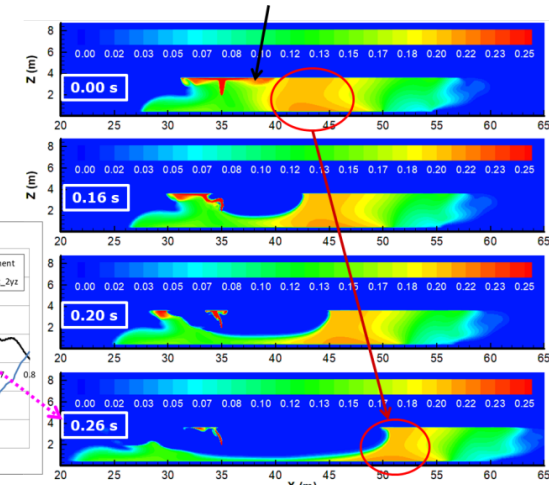
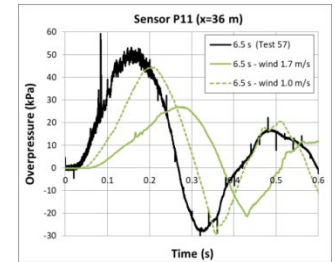
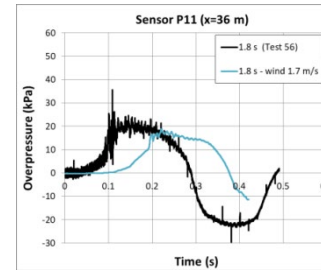
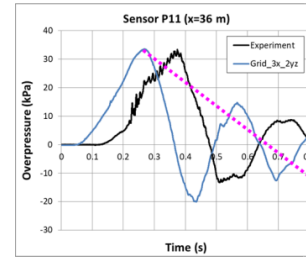
- Detailed grid independency study was conducted revealing that deflagrations results are particular sensitive to grid changes.
  - 3.8 million cells to achieve satisfactory grid independency
- The agreement between simulation results and measurements was very good in the forced ventilation case.
- Simulation results reveal that only the hydrogen that exists in 5 m radius (1.5 times the tunnel height) from the ignition point contributes to maximum overpressure.
- Small changes in wind speed can have significant changes in overpressure. The higher the wind is the lower the overpressure is.
- About the experiments with different ignition delay, good agreement is achieved in the 0.0 s and 1.8 s cases. In the 6.5 s case the overpressure is predicted better when using wind speed equal to 1.0 m/s.



# Ευχαριστώ! (Thank you)



## Questions



**Acknowledgements:** The research leading to these results was financially supported by the **HyTunnel-CS** which has received funding from the Fuel Cells and Hydrogen 2 Joint Undertaking under grant agreement No 826193

The authors would like also to acknowledge the Greek Research & Technology Network (GRNET) for the computational time granted us in the Greek National HPC facility ARIS (<http://hpc.grnet.gr>) under project H2TUN (pr014025)



## FUEL CELLS AND HYDROGEN JOINT UNDERTAKING



European  
Commission

Horizon 2020  
European Union funding  
for Research & Innovation