

# TOWARDS THE SIMULATION OF HYDROGEN LEAKAGE SCENARIOS IN CLOSED BUILDINGS USING CONTAINMENTFOAM

19. SEPTEMBER 2023 I KHALED YASSIN, STEPHAN KELM, AND ERNST-ARNDT REINECKE







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### Motivation

The Living Lab Energy Campus project at FZ Jülich











# **MOTIVATION**

#### Towards Net Zero Carbon by 2050 – the required hydrogen production



17-Sep-23

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# **MOTIVATION**

Safety concerns for indoor hydrogen use



How GH<sub>2</sub> behave in case of leakage?

> How to extract GH<sub>2</sub> from space in case of leakage?

Where to locate the sensors for proper GH<sub>2</sub> detection?



# THE LIVING LAB ENERGY CAMPUS (LLEC) AT FZ JÜLICH

#### General overview: PtG++ sub project



**LOHC** Liquid Organic Hydrogen Carrier



# THE LIVING LAB ENERGY CAMPUS (LLEC) AT FZ JÜLICH

#### The central utility building at Jülich campus



### CFD libraries containment $\nabla F$ ( $\Re$ AM

- Flows and Transport Phenomena [1]
  - Efficient Multi-Species Solver: effective binary diffusion, Wilke mixture
  - Turbulence transport:  $k-\omega$  SST model with buoyancy terms,
  - PARs: Code coupling with mechanistic model REKODIREKT
  - o Burst discs, flaps, doors: conditional mesh interfaces
  - Code coupling with OpenModelica
  - Conjugate heat transfer, Wall condensation, Fog formation, Gas radiation, Aerosol transport, Technical Systems and Components, porous media
- The codes are extensively validated against different experiments in nuclear and hydrogen applications [2]
  Transferring experience in nuclear safety to hydrogen safety



Steam distribution inside the containment, 3D CAD Geometry by [L. Serra-Lopez (UPM)]

 [1] Kelm, S. et al. "The Tailored CFD Package 'containmentFOAM' for Analysis of Containment Atmosphere Mixing, H<sub>2</sub>/CO Mitigation and Aerosol Transport, *Fluids* (2021) 6, no. 3: 100.
[2] Yassin, K.; Kelm, S.; Kampili, M.; Reinecke, E.-A. Validation and Verification of containmentFOAM CFD Simulations in Hydrogen Safety. *Energies* 2023, *16*, 5993. https://doi.org/10.3390/en16165993



#### **Scenarios**



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#### **Simulation parameters**



![](_page_8_Picture_3.jpeg)

No ventilation vs Mechanical - cloud development (contour surface represents the LFL surface) After 5 s

![](_page_9_Picture_2.jpeg)

![](_page_9_Picture_3.jpeg)

### No ventilation vs Mechanical After 15 s

![](_page_10_Picture_2.jpeg)

![](_page_10_Picture_3.jpeg)

### No ventilation vs Mechanical After 20 s

![](_page_11_Picture_2.jpeg)

![](_page_11_Picture_3.jpeg)

### No ventilation vs Mechanical After 40 s

![](_page_12_Picture_2.jpeg)

![](_page_12_Picture_3.jpeg)

![](_page_13_Figure_1.jpeg)

![](_page_13_Figure_2.jpeg)

![](_page_13_Figure_3.jpeg)

![](_page_13_Picture_4.jpeg)

Mechanical vs Natural Ventilation - cloud development (contour surface represents the LFL surface 4%) After 5 s

![](_page_14_Picture_2.jpeg)

![](_page_14_Picture_3.jpeg)

#### Mechanical vs Natural Ventilation After 15 s

![](_page_15_Picture_2.jpeg)

![](_page_15_Picture_3.jpeg)

#### Mechanical vs Natural Ventilation After 20 s

![](_page_16_Picture_2.jpeg)

![](_page_16_Picture_3.jpeg)

#### **Mechanical vs Natural ventilation - cloud development**

![](_page_17_Figure_2.jpeg)

![](_page_17_Figure_3.jpeg)

![](_page_17_Picture_4.jpeg)

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Volume of combustible cloud (i.e.  $H_2 = 4\%-75\%$  vol.)

![](_page_18_Figure_2.jpeg)

![](_page_18_Picture_3.jpeg)

![](_page_19_Figure_1.jpeg)

![](_page_19_Picture_2.jpeg)

#### New proposed locations for exhaust outlets

![](_page_20_Picture_2.jpeg)

![](_page_20_Picture_3.jpeg)

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#### Volume of combustible cloud with the new proposed locations

![](_page_21_Figure_2.jpeg)

![](_page_21_Picture_3.jpeg)

# CONCLUSIONS

### The main player in hydrogen cloud dispersion is the buoyancy force

- Natural ventilation from the ceiling is (usually) the most effective
- Exhaust outlets should be in the ceiling or as close as possible to it
- There should be no obstacles between potential hydrogen leakage source and the ceiling
- Overhead structures (ex.: Pipes) tend to break up the cloud which enhances mixing with the air, which increases the cloud volume
- Hydrogen tend to accumulate near the corners between walls and the ceiling
- More studies should be done to study the proper mechanical ventilation rates

![](_page_22_Picture_8.jpeg)

# **FUTURE WORK**

- Effects of different leakage locations and directions
- Optimizing sensors' locations
- Studying the usage of catalytic passive autocatalytic Recombiners (PARs) to mitigate hydrogen accumulation and dispersion in the building

![](_page_23_Picture_4.jpeg)

- The Living Lab Energy Campus (LLEC) Power to Gas (PtG++) project is funded by the German Federal Ministry of Education and Research (BMBF) project No.:03SF0573.
- Simulations were carried out using Jülich Super Computer (JSC) for the project grant No. 26701

Contact: k.yassin@fz-juelich.de

![](_page_24_Picture_3.jpeg)

![](_page_24_Picture_4.jpeg)

## Thank you for your attention !! Questions?

![](_page_24_Picture_6.jpeg)

![](_page_25_Picture_0.jpeg)

![](_page_25_Picture_1.jpeg)

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### **COMPUTATIONAL GRID**

![](_page_26_Picture_1.jpeg)

![](_page_26_Picture_2.jpeg)

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# **INITIAL AND BOUNDARY CONDITIONS**

Variable	External walls		Internal walls		Air inlet		Atmosphere		Exhaust outlets		Domain linit
	BC	Init.	BC	Init.	BC	Init.	BC	Init.	BC	Init.	
р	fixedFluxPresure	1 bar	fixedFluxPresure	1 bar	inletOutlet	1 bar	inletOutlet	1 bar	fixedFluxPresure	1 bar	1 bar
Т	zeroGradient	-	zeroGradient	-	inletOutlet	298.15 K	inletOutlet	298.15 K	zeroGradient	-	298.15 K
U	No slip	(0,0,0)	No slip	(0,0,0)	inletOutlet	(0,0,0)	inletOutlet	(0,0,0)	Flow Rate Velocity	0.48567, 1.543 m3/s	
nut	SpaldingWall Function	1.00E-07	SpaldingWall Function	1.00E-07	inletOutlet	1.00E-07	inletOutlet	1.00E-07	calculated	1.00E-07	1.00E-07
k	kqR Wall Function	1.35E-05	kqR Wall Function	1.35E-05	inletOutlet	1.35E-05	inletOutlet	1.35E-05	zeroGradient	1.35E-05	1.35E-05
ω	omega Wall Function	1.00E-07	omega Wall Function	1.00E-07	inletOutlet	1.00E-07	inletOutlet	1.00E-07	zeroGradient	1.00E-07	1.00E-07
H <sub>2</sub>	zeroGradient	-	zeroGradient	-	inletOutlet	0	inletOutlet	0	zeroGradient	-	0
0 <sub>2</sub>	zeroGradient	-	zeroGradient	-	inletOutlet	0.2328	inletOutlet	0.2328	zeroGradient	-	0.2328
N <sub>2</sub>	zeroGradient	-	zeroGradient	-	inletOutlet	0.7672	inletOutlet	0.7672	zeroGradient	-	0.7672

![](_page_27_Picture_2.jpeg)

# NUMERICAL SOLVERS, SCHEMES, AND CONVERGENCE CRITERIA

Variable	Solutio	on	div Schomo		
variable	Solver	tol.			
р	GAMG	1.00E-06	Gauss upwind		
Т	PBiCGStab	1.00E-06	Gauss upwind		
U	PBiCGStab	1.00E-06	Gauss linearUpwind grad(U)		
nut	PBiCGStab	1.00E-06	Gauss linear		
k	PBiCGStab	1.00E-06	Gauss upwind		
ω	PBiCGStab	1.00E-06	Gauss upwind		
H <sub>2</sub>	PBiCGStab	1.00E-06	Gauss upwind		
O <sub>2</sub>	PBiCGStab	1.00E-06	Gauss upwind		
N <sub>2</sub>	PBiCGStab	1.00E-06	Gauss upwind		

Time	Euler
Grad.	cellMDLimited Gauss linear 0.5
Laplacian	Gauss linear limited 0.5
Interpol.	linear

![](_page_28_Picture_3.jpeg)

# **TURBULENCE MODEL**

k-ω SST with Simple Gradient Diffusion Hypothesis (SGDH)

$$\begin{aligned} \frac{\partial \rho}{\partial t} + \nabla \cdot \left(\rho \vec{U}\right) &= 0\\ \frac{\partial \rho \vec{U}}{\partial t} + \nabla \cdot \left(\rho \vec{U} \otimes \vec{U}\right) &= -\nabla p + \nabla \cdot \tau + \rho \vec{g}\\ \frac{\partial \rho h_{tot}}{\partial t} + \nabla \cdot \left(\rho \vec{U} h_{tot}\right) &= \frac{\partial p}{\partial t} - \nabla \cdot \vec{q}'' + \nabla \cdot (\vec{U} \cdot \tau) + \vec{U} \cdot (\rho \vec{g}) - \nabla \cdot \vec{q}''_{rad}\\ \frac{\partial \rho Y_i}{\partial t} + \nabla \cdot \left(\rho \vec{U} Y_i\right) &= -\nabla \cdot \vec{J}_i \end{aligned}$$

![](_page_29_Picture_3.jpeg)

# **TURBULENCE MODEL**

k-ω SST with Simple Gradient Diffusion Hypothesis (SGDH)

$$\begin{split} \frac{\partial \left(\rho k\right)}{\partial t} + \nabla \cdot \left(\rho \vec{U}k\right) &= \nabla \cdot \left(\left(\mu + \mu_t \sigma_k\right) \nabla k\right) + \tilde{P}_k - \rho \beta^* \omega k + P_{k,b} \\ \frac{\partial \left(\rho \omega\right)}{\partial t} + \nabla \cdot \left(\rho \vec{U}\omega\right) &= \nabla \cdot \left(\left(\mu + \mu_t \sigma_\omega\right) \nabla \omega\right) + 2\left(1 - F_1\right) \frac{\rho \sigma_{\omega 2}}{\omega} \nabla k \cdot \nabla \omega + P_\omega + P_{\omega,b} - Y_\omega \\ P_{\omega,b} &= \nu_t ((\gamma + 1)C_3 \cdot max(P_{k,b}, 0) - P_{k,b}) \\ P_{k,b} &= -\frac{\nu_t}{\sigma_\rho} g_i \frac{\partial \rho}{\partial x_i} \end{split}$$

![](_page_30_Picture_3.jpeg)

# VALIDATION AND VERIFICATION: FLAME EXP.

![](_page_31_Figure_1.jpeg)

O'hern, T. J., Weckman, E. J., Gerhart, A. L., Tieszen, S. R., & Schefer, R. (2005). Experimental study of a turbulent buoyant helium plume. *Journal of Fluid Mechanics*, *544*, 143-171.

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# VALIDATION AND VERIFICATION: FLAME EXP.

![](_page_32_Figure_1.jpeg)

Swain, M. R., Grilliot, E. S., & Swain, M. N. (1998). *Risks incurred by hydrogen escaping from containers and conduits* (No. NREL/CP-570-25315-Vol. 2; CONF-980440-Vol. 2). National Renewable Energy Lab.(NREL), Golden, CO (United States).

![](_page_32_Picture_3.jpeg)

#### Natural ventilation - cloud phenomena after 20 s

### High concentrations at corners

![](_page_33_Figure_3.jpeg)

# **MOTIVATION**

#### But...hydrogen has extreme physical properties

![](_page_34_Figure_2.jpeg)

Kotchourko, A. and Jordan, T. eds., 2022. Hydrogen Safety for Energy Applications: Engineering Design, Risk Assessment, and Codes and Standards. Butterworth-Heinemann.
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![](_page_34_Picture_4.jpeg)

Phenomena occurring during GH2 leakage

![](_page_35_Figure_2.jpeg)

![](_page_35_Picture_3.jpeg)

# THE LIVING LAB ENERGY CAMPUS (LLEC) AT FZ JÜLICH

#### Scope of work

![](_page_36_Figure_2.jpeg)

![](_page_36_Picture_3.jpeg)

# **MOTIVATION**

![](_page_37_Figure_1.jpeg)

Remove the first motivation slide Say more about the building and its complixty We are transferring experience from Nuclear applications to Hydrogen applications

![](_page_38_Picture_1.jpeg)