



Designing an inherently safe H₂ infrastructure:

Combining analytical, experimental, and numerical investigations to optimize H₂ refueling stations safety by passive mitigation

Deborah Houssin-Agbomson | *AL R&D*

Audrey Herzig, Andrew Autuore, Mike Molesworth, Victor Riso, Ajay Prasad | *UD*

Aurélien Soubeyran, Bo Lu, Zehao Wei | *AL R&D*

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Context



Context & Objectives

■ Context

Clean Hydrogen and **Fuel Cell Electric Vehicles (FCEV)** have developed significantly in the past years in order to respond appropriately to the challenges associated with the **transition to a Net-Zero Carbon Economy**

Associated infrastructure, in particular, **Hydrogen Refueling Stations (HRS)** were also developed to respond to the **increasing needs for Hydrogen in the mobility** sector

■ Challenges

The need to mainstream Hydrogen in the mobility sector requires **higher levels of accessibility of HRS** in the **public environment**

Thus, it is necessary to **deploy inherently safe hydrogen refueling stations** without increasing **footprint** of such infrastructure because of excessively **drastic safety distances and barriers**

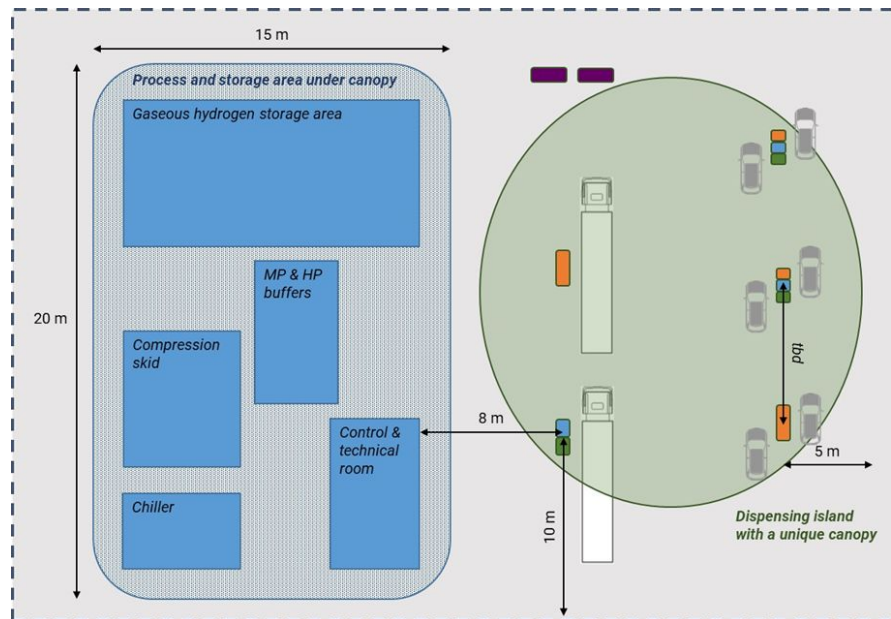
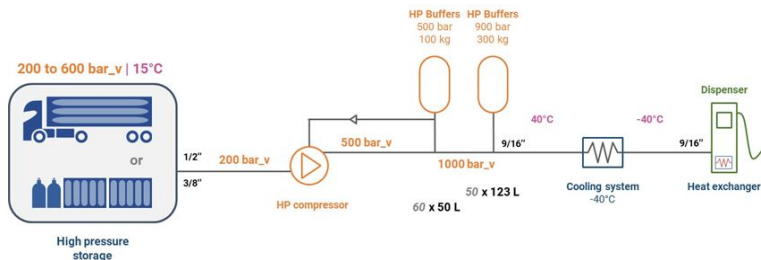
■ Study objectives

Combine **design**, conception and **aesthetic** of HRS for a **better integration in urban environment**

⇒ while keeping **safety consideration as the top priority**

Gas-to-Gas H₂ Refueling Station

Generalities & Scope of the study



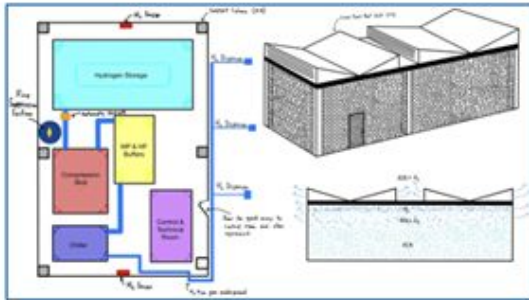
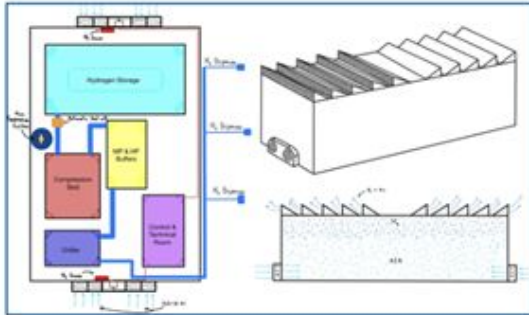
■ Focus on confined parts of the HRS

- Processing container
- Dispenser

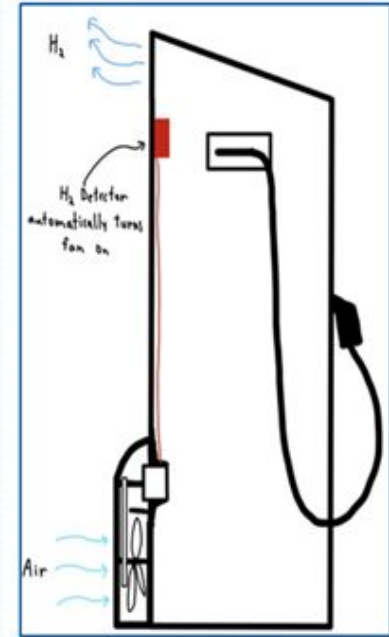
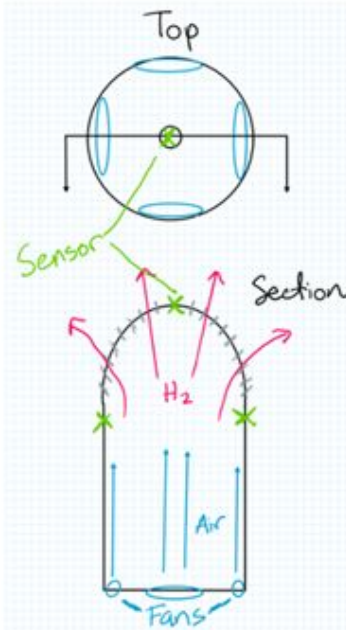
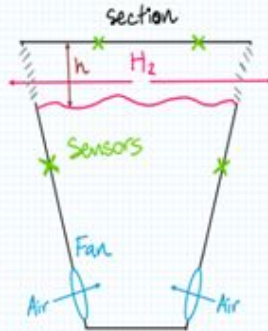
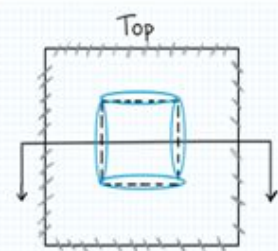
Design concepts

Ideation

Processing container

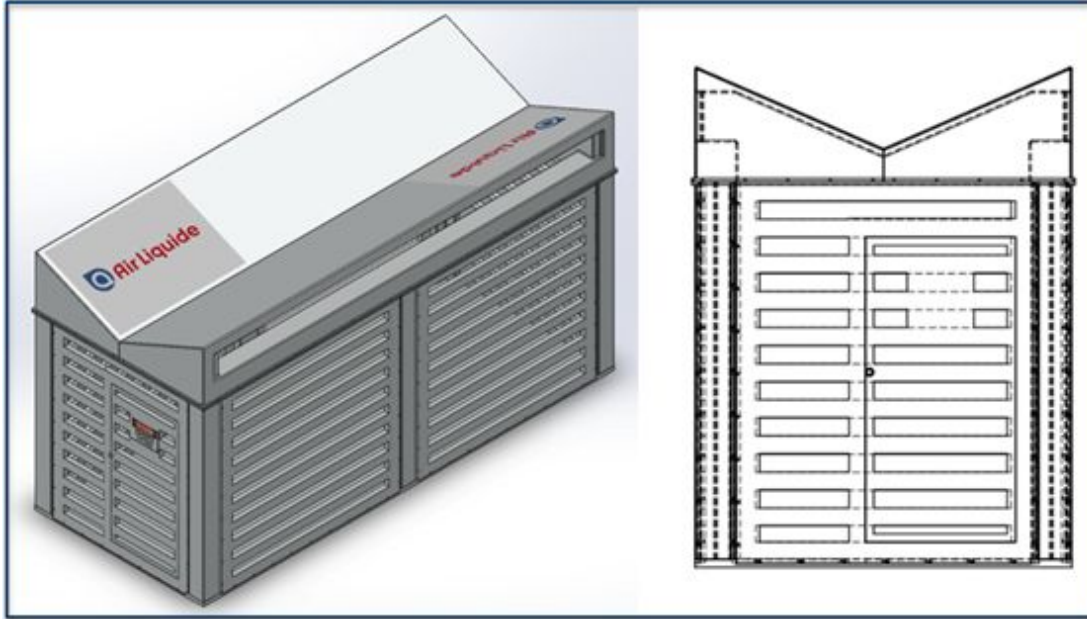


Dispenser



Concepts retained

Criteria & Final choice



Processing container → *louvered walls and v-shaped roof*

■ Criteria

- significantly different from existing
- assessable concept
- not too much costly
- easy-to-deploy
- time-to-market considerations

Dispenser → *conical*



How to assess Risk & Safety — of the concepts?

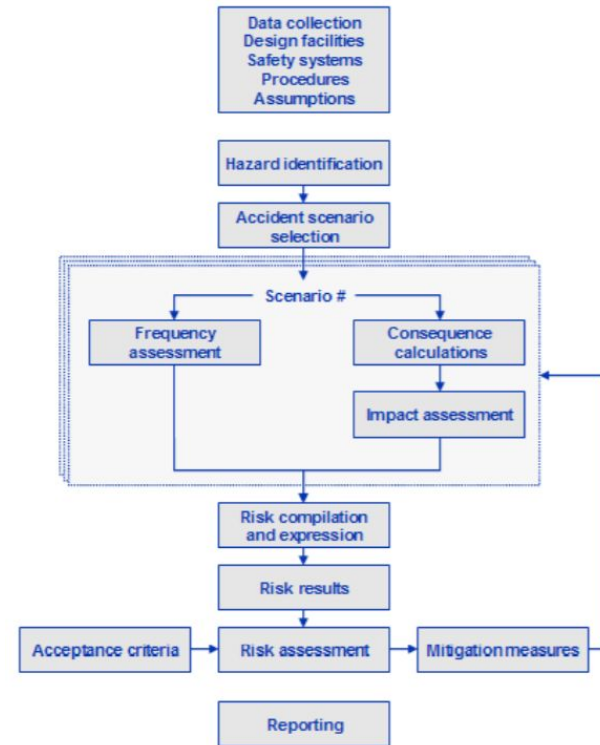
Concrete cases

Risk analysis & consequences assessment - Methodologies and generic calculations

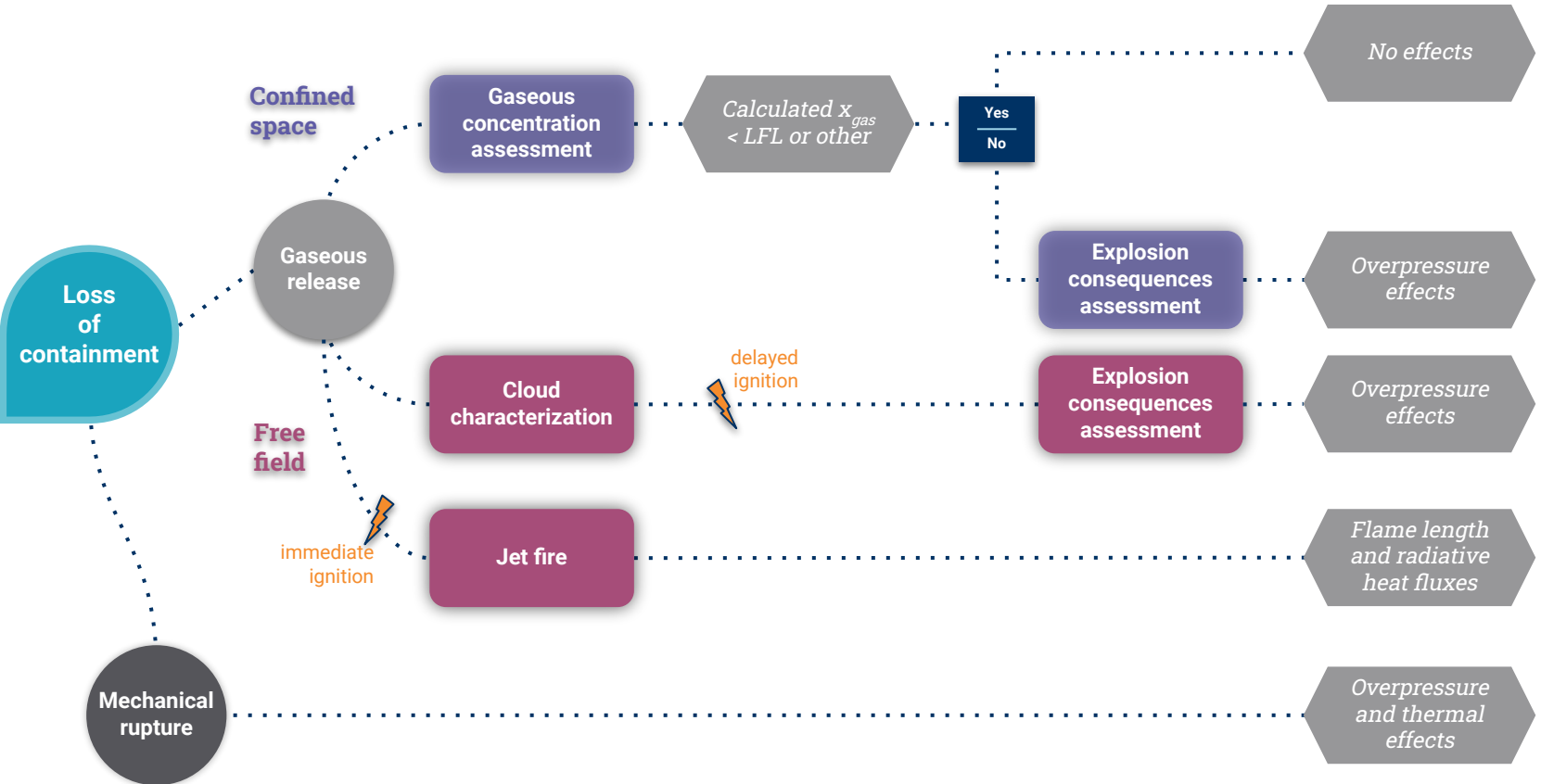
- 1 Description of the studied case
- 2 Hazard identification
- 3 Severity assessment
- 4 Interpretation & Mitigation
- 5 Final design

Potential safety requirements in RCS, but:

- **no specification on how to assess the severity of a feared event**
- **and rarely definition on methods/means to respect these requirements...**



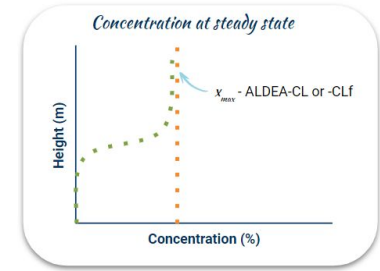
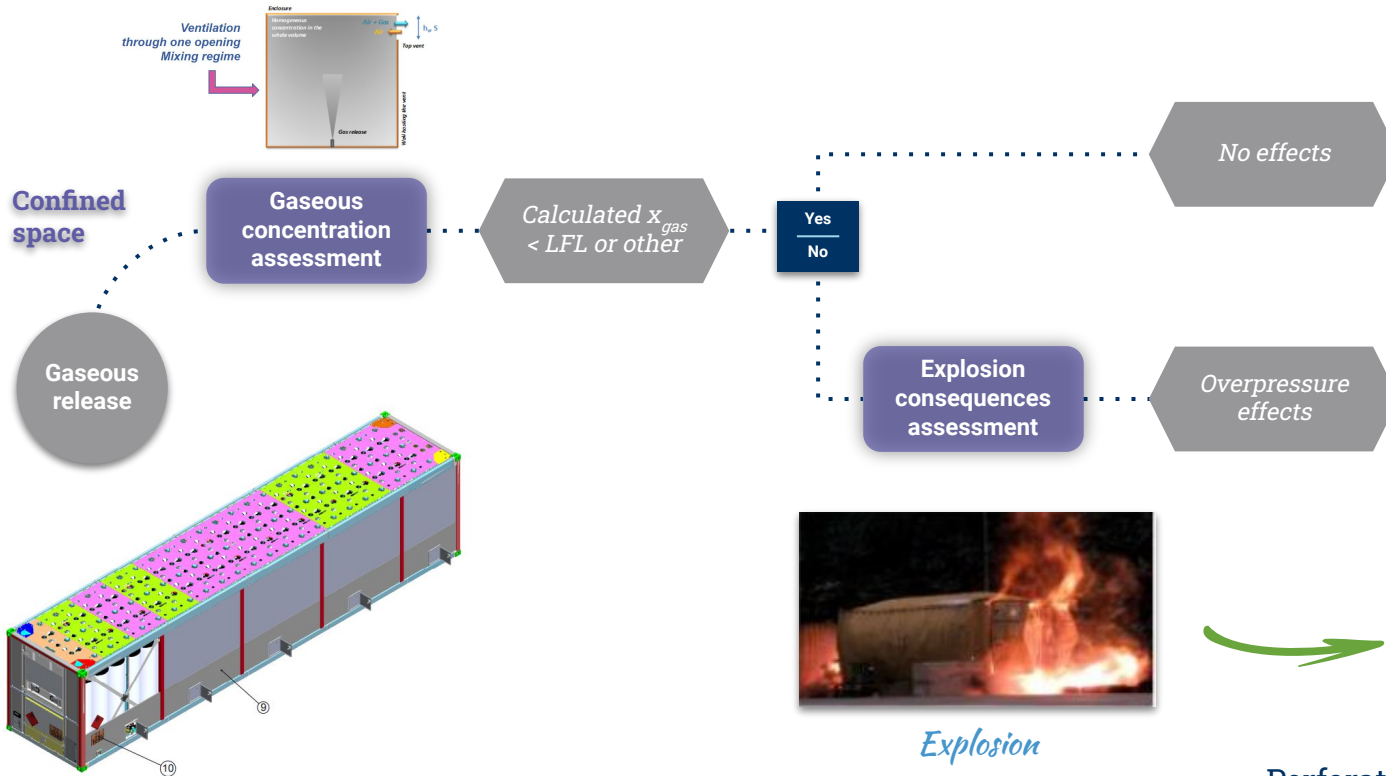
Identification of the phenomena and associated consequences



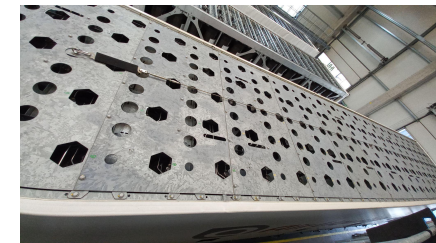
Risk analysis and Mitigation means proposal

Manage internal accidental releases

Smart natural ventilation



Build-up



Means for Severity assessment — of feared events

Existing assessment means

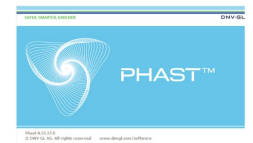
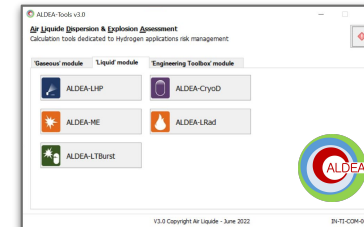
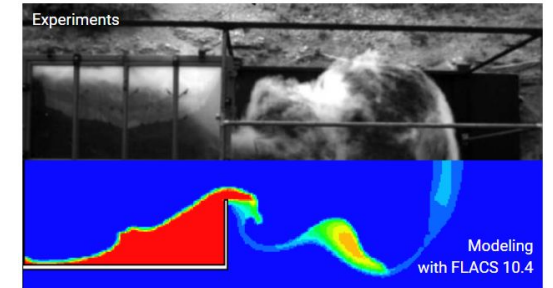
Non-exhaustive list

■ Complementary approaches

- **Analytical modelling** | *HyRAM, PHAST, e-laboratory, non-public tools...*
(ALDEA for AL)
For quick and simple calculations
- **Numerical simulations (CFD)** | *FLACS, FLUENT...*
For complex geometries and scenarios, numerical experiments, extrapolation
- **Experiments** | *Several test facilities and collaborative platforms*
For validation and specific scenarios

and... Define and Evaluate mitigation means

- Concepts, Equipment, Protocols...



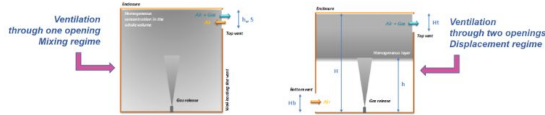
Evaluation — of dispenser concepts

Dispenser concept

Studied cases

Method

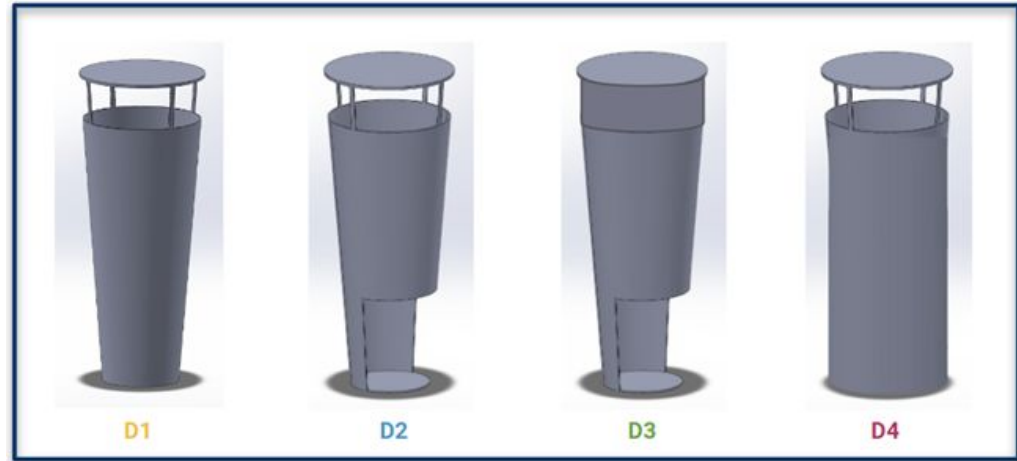
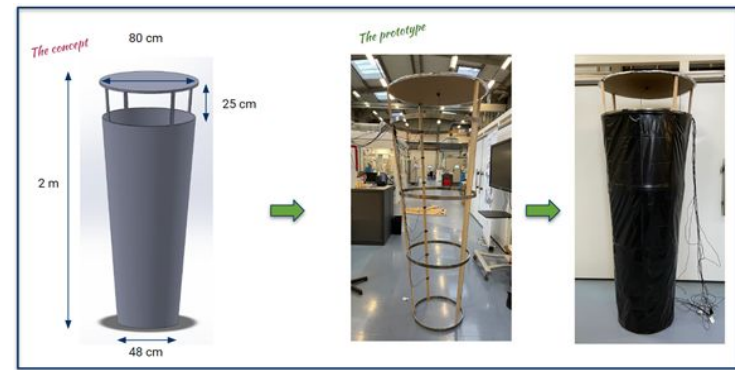
- Pre-calculations with analytical approaches to size the Dispenser mock-up (Linden 1999)



- Build-up experiments with natural ventilation
Concentration distribution thanks to minicatharometers in **near-real scale mock-up**
 - with He flow rates from 5 to 100 NL.min⁻¹
 - for different variants of the design

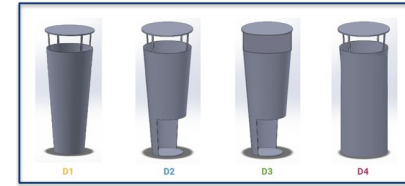


- Extrapolation with numerical simulations
 - for 120 g.s⁻¹ which is commonly the maximum flow rate in a dispenser



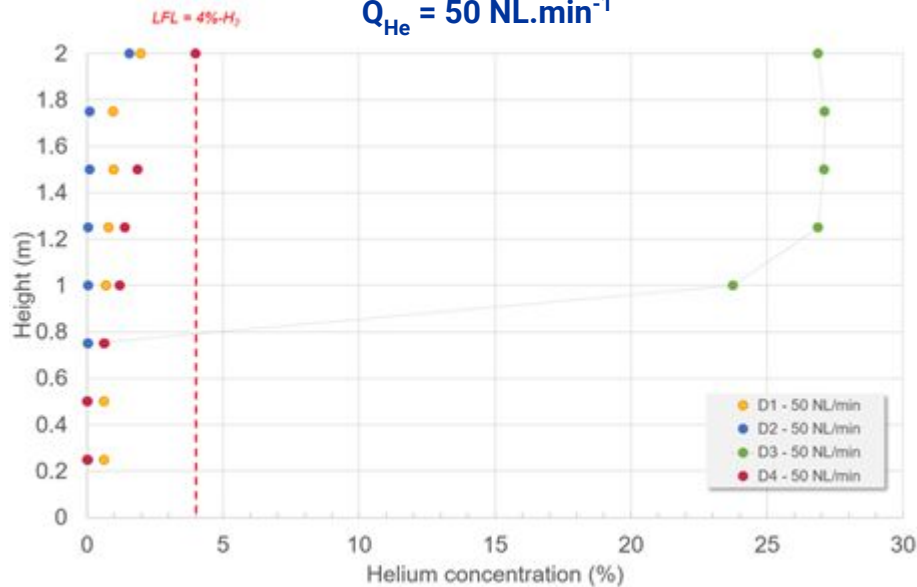
Dispenser concept

Experimental results

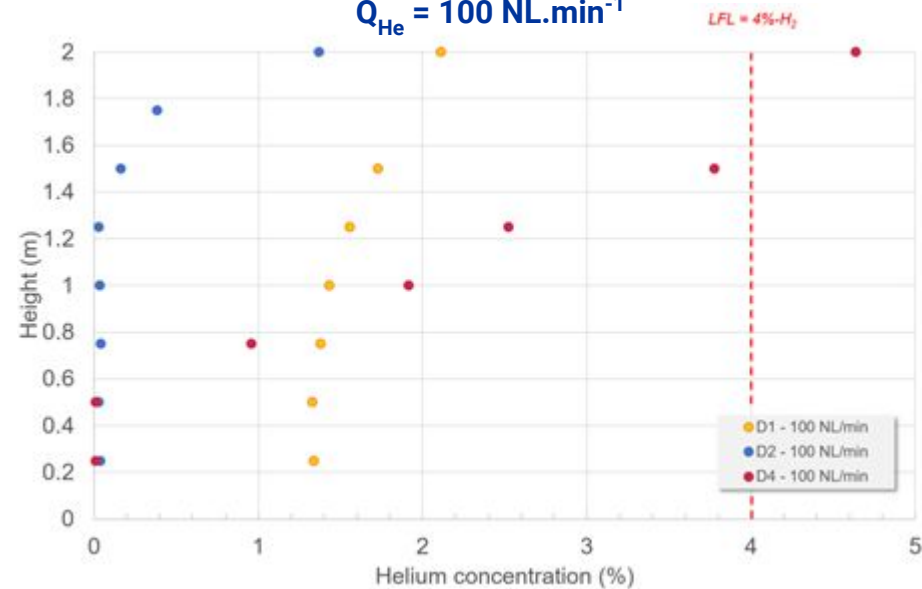


- Design comparison → for 50 and 100 NL.min⁻¹
Concentration profiles at steady state

$Q_{He} = 50 \text{ NL.min}^{-1}$



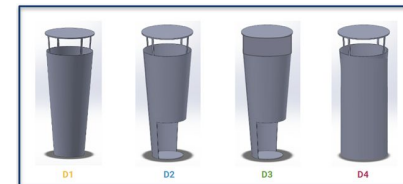
$Q_{He} = 100 \text{ NL.min}^{-1}$



⇒ Ventilation mode and design of **D2-dispenser** give the best performances, i.e. the lowest concentrations, contrarily to D3-dispenser

Dispenser concept

Overview of experimental measurements vs analytical calculations



- **Maximum concentrations** → from 5 and 100 NL.min⁻¹ at steady state

Release flow rates		5 NL.min ⁻¹		50 NL.min ⁻¹		100 NL.min ⁻¹	
<i>Approach</i>		<i>Exp.</i>	<i>Linden</i>	<i>Exp.</i>	<i>Linden</i>	<i>Exp.</i>	<i>Linden</i>
D1-dispenser		0.8%	0.5%	2%	2.4%	2.3%	3.8%
D2-dispenser		0.7%	0.3%	1.3%	1.4%	1.4%	2.3%
D3-dispenser		6.3%	-	26%	-	36%	-
D4-dispenser		0.8%	0.8%	N/A	2.4%	4.5%	5.6%

- ⇒ At **highest flow rates**, **Linden** approach **over-predicts maximum concentration**
For same ventilation areas, **conical shape (D1)** is **more efficient** than cylindrical dispenser (D4)

Dispenser concept

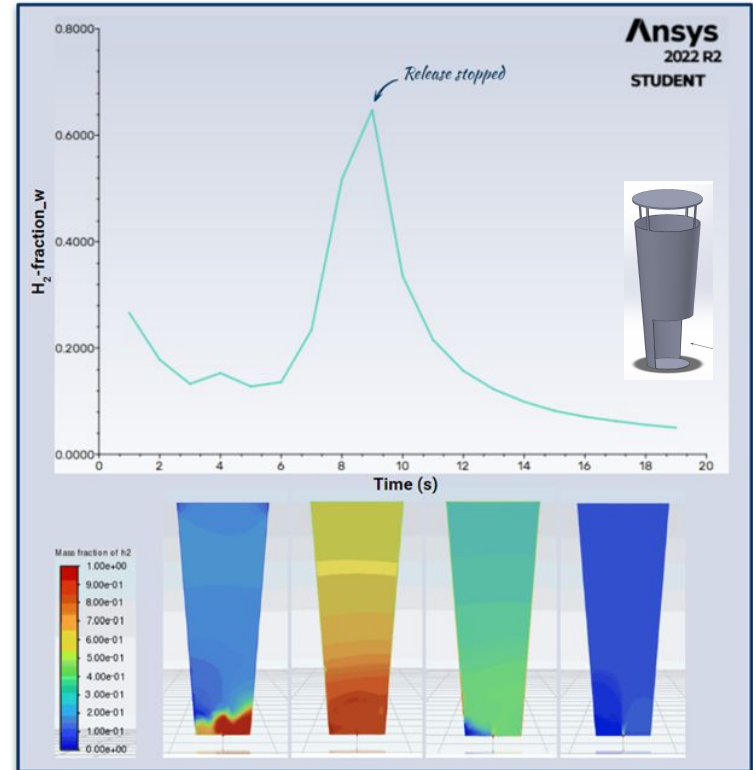
Extrapolation with numerical calculations

- Preliminary investigations with D2-dispenser for $120 \text{ g}\cdot\text{s}^{-1}$ release rate
 - 30%- H_2 is largely exceeded
 - However, if the release is stopped, acceptable concentration levels are found in 10 s
 - In case of ignition at stoichiometry (30%- H_2), considering ventilation opening as explosion venting panels, maximum internal overpressure would be lower than 50 mbar (calculated by Molkov et al. approach (1999)) → inducing deformation of the dispenser but no destruction, and no or limited fragments

(coming... interesting experiments on ignition of flammable mixtures in a dispenser led by HSE in the framework of MultHyFuel project)

⇒ These results are very preliminary and will be refined for the next steps of this collaborative research work

- Need of more validation, a better calibration of the numerical model and associated parameters with an expert



Evaluation — of processing container concepts

Processing container concept

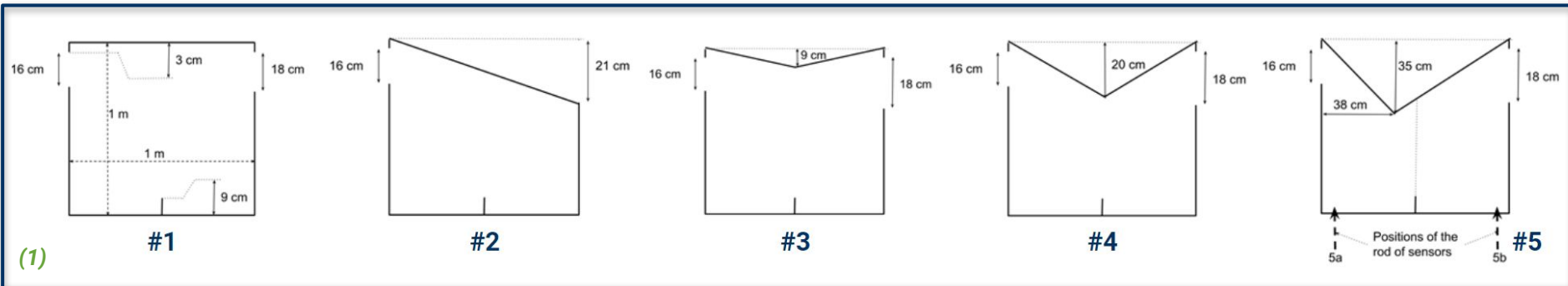
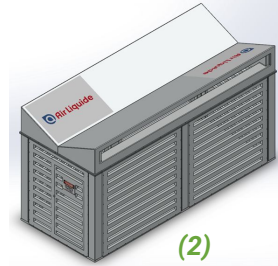
Studied cases

Method

- Investigations in two-steps: first on **roof inclination (1)**, and after combination of **inclined roof and louvered walls (2)**
- Build-up experiments** with natural ventilation
Concentration distribution thanks to minicatharometers in a 1-m³ enclosure
 - with He flow rates from 5 to 100 NL.min⁻¹
 - for different variants of the design
- Experimental investigations on visualization of ventilation fluxes paths
 - with immersed down scaled mock-up - Archimedes number approach
 - with smokes outside the enclosure
- Further investigations with **SimScale online numerical tool**

Back to the concept





- Roof inclination & Louvered walls** for natural ventilation and build-up mitigation



Processing container concept

Experimental measurements / Roof inclination

- **Maximum concentrations in a 1-m³ enclosure** → from 5 and 100 NL.min⁻¹ at steady state

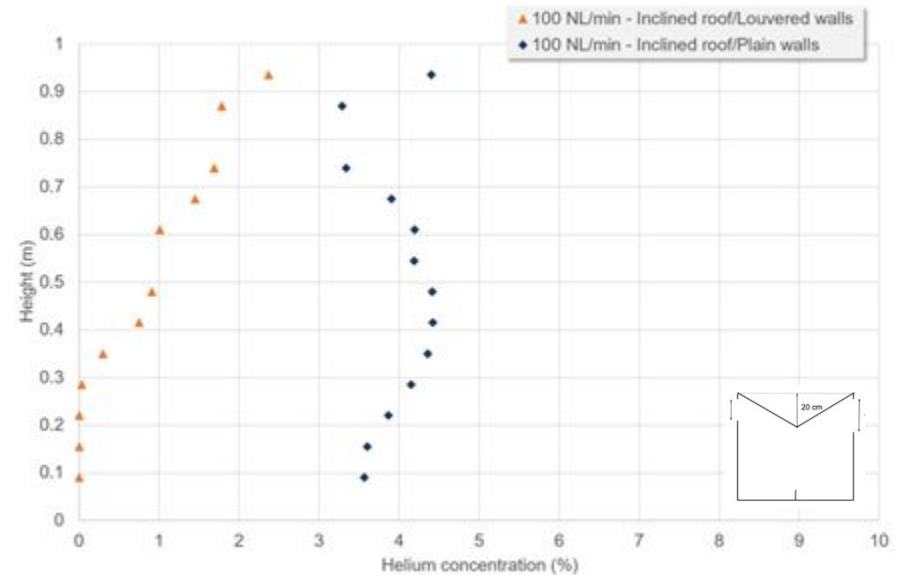
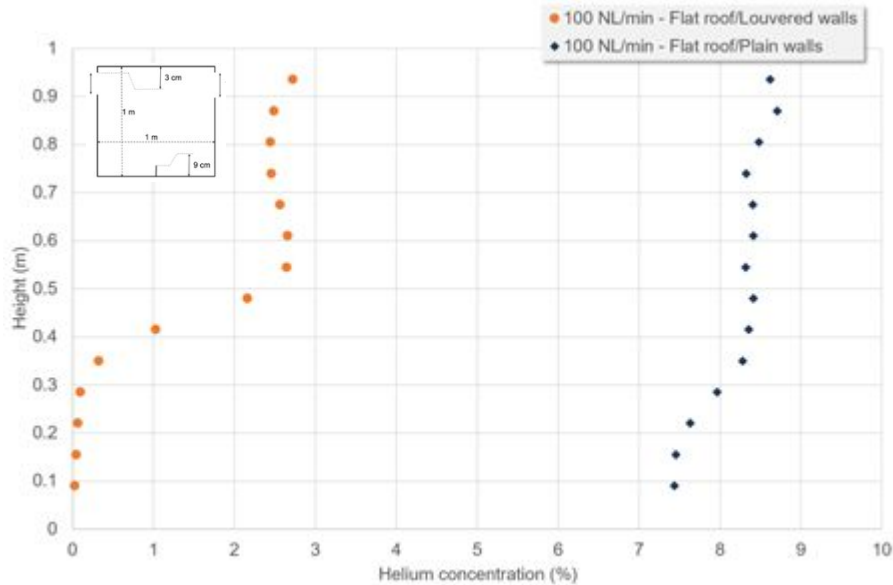
Release flow rates		5 NL.min ⁻¹	20 NL.min ⁻¹	50 NL.min ⁻¹	100 NL.min ⁻¹
Configuration 1	 0%	1.4%	2.5%	4%	8.5%
Configuration 2		1.6%	3.8%	7%	14%
Configuration 3	 18%	0.8%	2.1%	3.9%	7.5%
Configuration 4	 40%	0.8%	2%	3.5%	4.5%
Configuration 5a	 a b	0.3%	1.4%	3%	1.5%
Configuration 5b		1%	2.3%	5%	6%

- ⇒ **Double inclination** of the roof fosters He build-up mitigation
The more inclined the roof is, the lower the maximum concentration in the enclosure is

Processing container concept

Experimental measurements / Roof inclination & Louvered walls

- Design comparison → Louvered vs Plain walls & Flat vs Inclined roof for 100 NL.min⁻¹

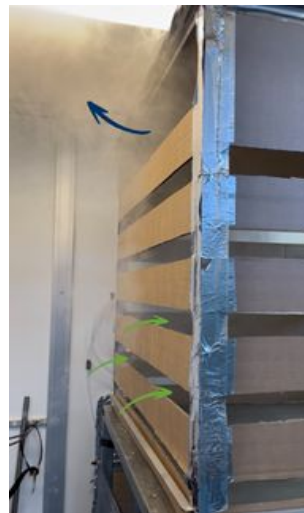


- ⇒ Louvered walls mitigate accumulation inside the container
- With louvered walls, positive impact of roof inclination on accumulation limitation is significantly reduced ($\pm 2.5\%$)
- Benefits of inclined roof are higher when walls are plain (4.5% vs 8.5%-He)

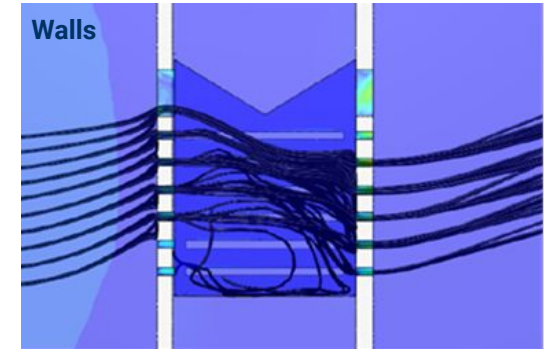
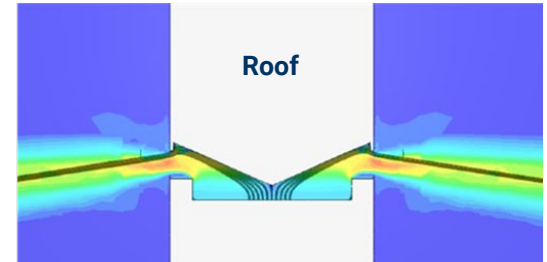
Processing container

Visualization of ventilation fluxes & Distribution

- Down scaled mock-up with Archimedes number approach
- Smokes with the 1-m³ enclosure



- Numerical simulation with SimScale



⇒ Inlet fluxes by vertical louvers
Outlet fluxes by the roof

Conclusions

Conclusions



- **A novel design concept was proposed by students from the University of Delaware for the hydrogen refueling stations by modifying physical structure**
 - A fruitful cross-disciplinary experience
- **Analytical, experimental and numerical approaches were combined in order to evaluate hydrogen concentration and distribution**
 - Significant positive effects on accumulation limitation in confined spaces - thanks to the specific studied designs - were demonstrated, with good agreement and complementarity between the investigated approaches
- **For the experimental part**
 - Helium was used as a surrogate of hydrogen in order to work safely
 - Near real-scale mock-ups were constructed for the dispenser study
 - Down-scaled mock-ups for the processing container
- **This work highlighted that analytical calculations using Linden approach - in most cases - overpredict the helium concentration compared to the results obtained experimentally**
- **Numerical simulation was investigated for dispenser and container topics**
 - Numerical simulations seem to match with experimental observations
 - However, at this stage, the preliminary results obtained are more qualitative than quantitative
 - Further work is required in order to be able to extrapolate the experimental results for other sizes and designs
 - Warning should be made about the use of CFD via tools available online; numerical simulations require expertise

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MOBILITY
by Air Liquide

Thank You

deborah.houssin@airliquide.com

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