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# **ID 204: Experimental Study on the Effect of the Ignition Location on Vented Deflagration of Hydrogen-Air Mixtures in Enclosure**

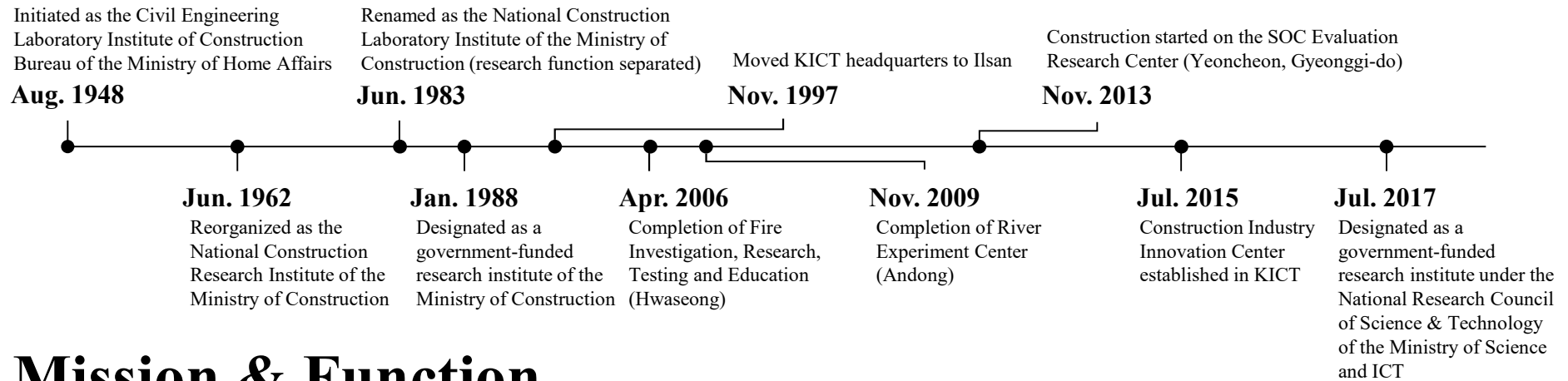
**2023. 09. 21.**

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**Hydrogen infrastructure research cluster,  
Korea Institute of Civil Engineering and Building Technology (KICT)**

**U.G. YOON**



# Mission & Function



The KICT contributes to the development of the Korean construction industry, improves quality of life standards, furthers national economic growth, and improves social welfare. We promote original technology in the fields of land, infrastructure, and construction.

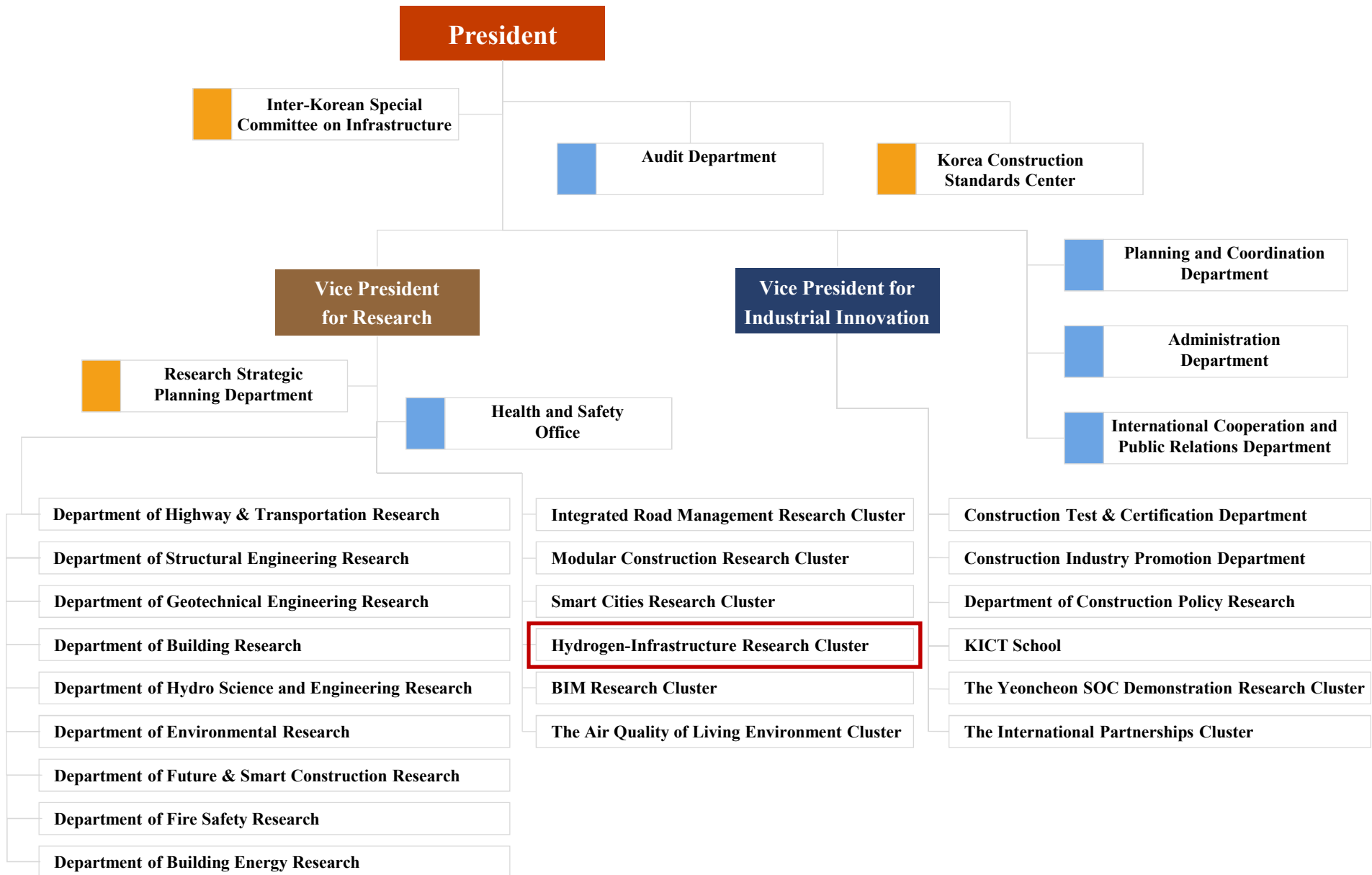


## Function

Research and Development

Policy-Making and Technology Support

Quality Certification and Testing Services



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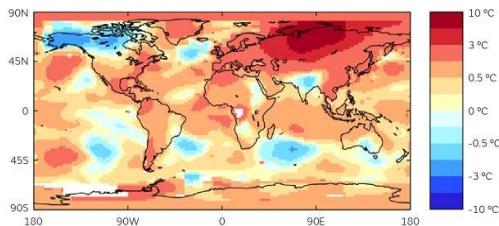
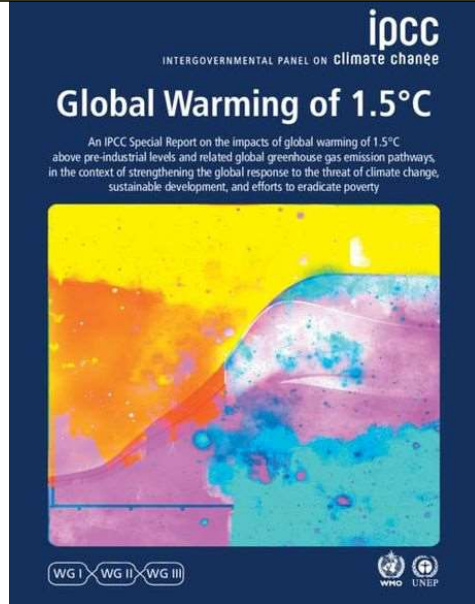
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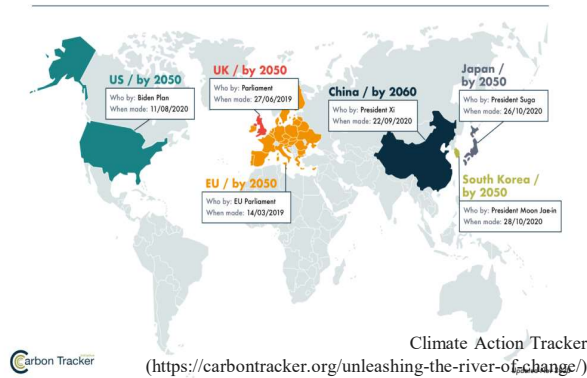
## 1.1 Background of research

### Special report on global warming of 1.5°C



The map using data from GISTEMP, Shows temperatures relative to the average between 1981-2010

### Key recent net zero policy commitments



### Hydrogen energy indispensable in the carbon neutrality era



Monthly people  
(<https://www.monthlypeople.com/news/articleView.html?idxno=270137>)

### The government announced the 「Hydrogen economy revitalization roadmap」 to lead the hydrogen economy

산업통상자원부		보도자료	
<a href="http://www.motie.go.kr">http://www.motie.go.kr</a>		보도자료	
2019년 1월 17일(목) 석간부터 보도하여 주시기 바랍니다. (인터넷, 방송, 통신은 1.17(목) 12:00 이후 보도 가능)			
배포일시	2019. 1. 16.(수)	담당부서	산업통상자원부 에너지산업과 기획재정부 혁신창업팀 과학기술정보통신부 원천기술과 환경부 대기환경과 국토교통부 미래전략일자리담당관 해수부 해사산업기술과
담당과장	신성필 과장(044-203-5390) 조원진 과장(044-215-4640) 김민표 과장(02-2110-2380) 박윤민 과장(044-201-6880) 백성호 과장(044-201-3258) 임현택 과장(044-200-5830)	담당자	박성수 사무관(044-203-5398) 장준희 사무관(044-215-4573) 손효진 사무관(02-2110-2758) 김건식 사무관(044-201-6887) 유훈 사무관(044-201-3260) 양진영 사무관(044-200-5834)

### 세계 최고수준의 수소경제 선도국가로 도약

- 정부, 「수소경제 활성화 로드맵」 발표 -

- ◇ 우리나라가 강점이 있는 '수소차'와 '연료전지'를 양대 축으로 수소경제를 선도할 수 있는 산업생태계 구축
- 수소차 누적 생산량을 '18년 2천대에서 '40년 620만대(내수 290만대, 수출 330만대)로 확대하고, 세계시장 점유율 1위 달성
- 국내 보급 : '17년 국내 177대(신규 51대) → '18년 누적 889대 (신규 712대) → '19년 4,000대 이상 신규 보급
- 수소충전소 확충 : ('18) 14개 → ('22) 310개 → ('40) 1,200개소
- 수소 대중교통 확대 : '40년 수소택시 8만대, 수소버스 4만대, 수소트럭 3만대 보급

- ❖ The Intergovernmental Panel on Climate Change (IPCC) proposed limiting global warming to 1.5°C above pre-industrial levels, which was adopted in the Paris Agreement, and limiting net carbon dioxide emissions by 2030 by 45% compared to 2010 and net zero by 2050.
- ❖ 121 countries around the world declared net zero by 2050 and 9 countries legislated net zero (as of Nov 2020).
- ❖ Korea also announced the Hydrogen Economy Roadmap to use hydrogen as a major source of energy (as of Jan 2019).

# 1. Introduction

## 1.2 Need for research



Hydrogen Infrastructure etc.



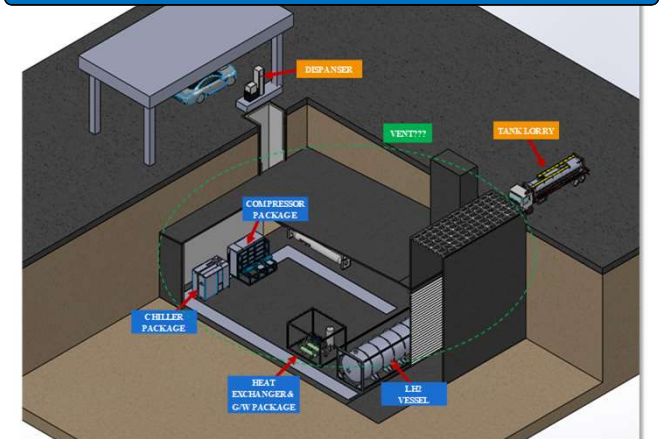
Gangneung venture plant hydrogen explosion accident site



Gunsan hydrogen plant explosion site



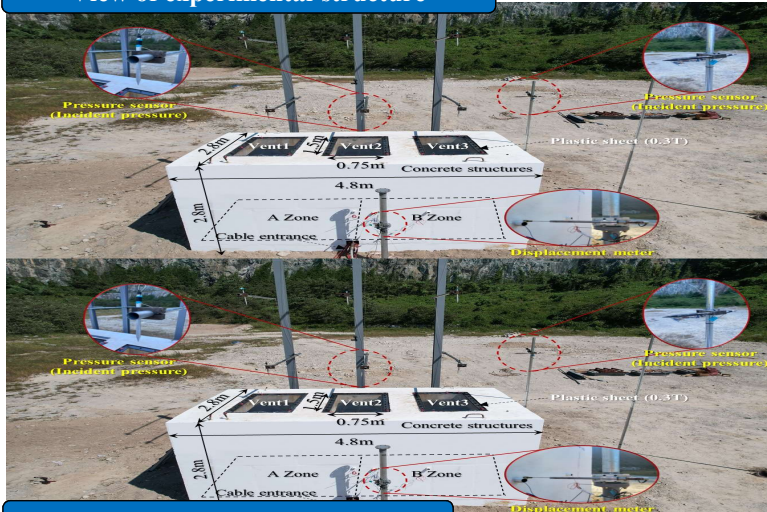
Underground liquefied hydrogen station layout (Plan)



- ❖ Hydrogen infrastructure is built mostly on the ground, which is limited in terms of obtaining enough space in city centers and adjacent areas and causes civil complaints in the city
- ❖ Lack of acceptance in terms of protection, rescue, and safety facilities to mitigate risk in facilities
- ❖ Lack of measures against potential hydrogen leaks, fires, or explosions in infrastructure, including safe distancing and facility specifications

## 1.3 Previous research and purpose of this study

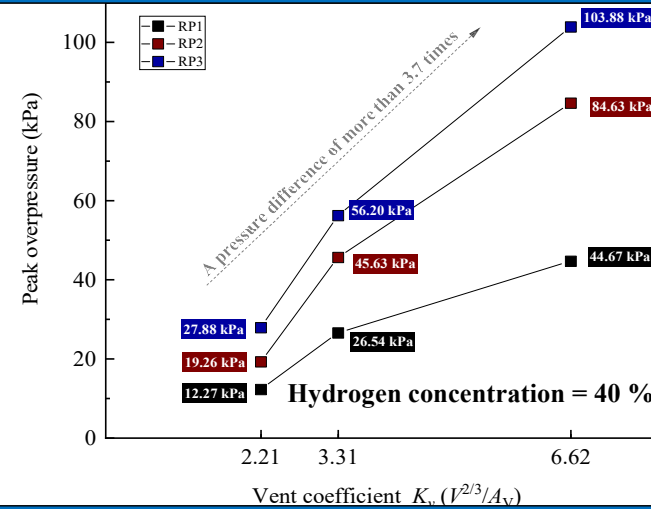
View of experimental structure



Vent conditions



Results of the peak overpressure according to the vent coefficient ( $K_v$ )

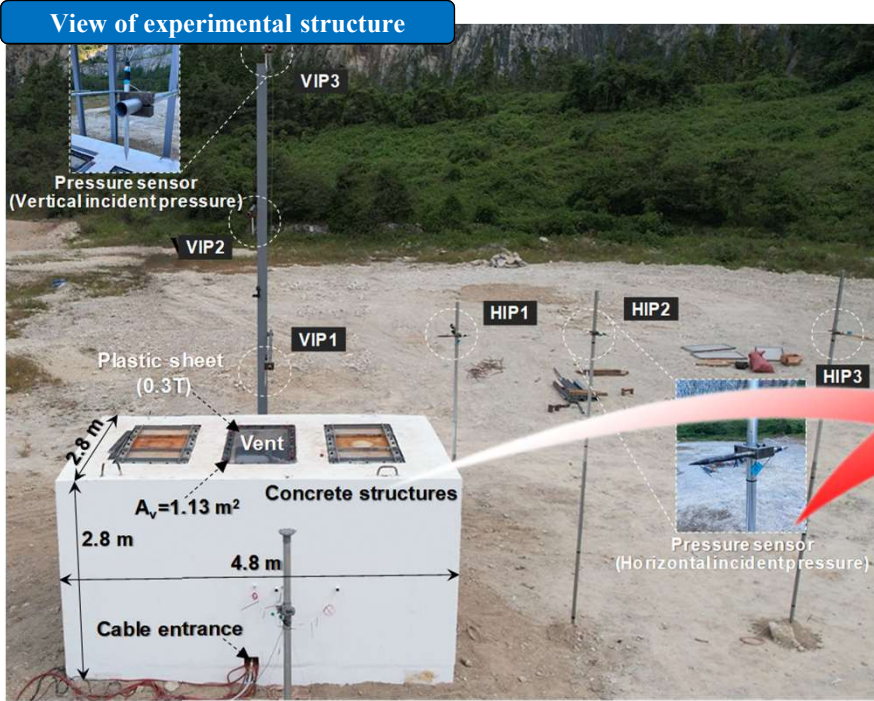


Airtight condition & hydrogen concentration 20%



- ❖ The previous research analyzed and confirmed **the damping effect of peak overpressure** depending on **the size of the vent** as an option to minimize **the impact of deflagration of hydrogen-air gas mixtures in an enclosure on people and buildings.**

## 2.1 Experimental structures and measuring instruments



- Overview of the experiment
- Experiment place: Army Corps of Engineers
  - Experiment structure: L:4.8m x W:2.8m x H:2.8m
  - Manufactured as a full-scale concrete structure with an internal volume of 20.3m<sup>3</sup>
  - Vent size: L:1.5m x W:0.75m
  - Vent design for opening and closing



Overview of experimental structure

Type	Structures							Roof vent		
	Dimensions (m)			Thickness (m)	Volume (m <sup>3</sup> )		Dimensions (m)		Area A (m <sup>2</sup> )	Coefficient $K_V (V^{2/3}/A_V)$
	L	W	H	W	Internal	External	L	H		
Concrete structures	4.8	2.8	2.8	0.3	20.33	37.63	0.75	1.5	1.13	6.62

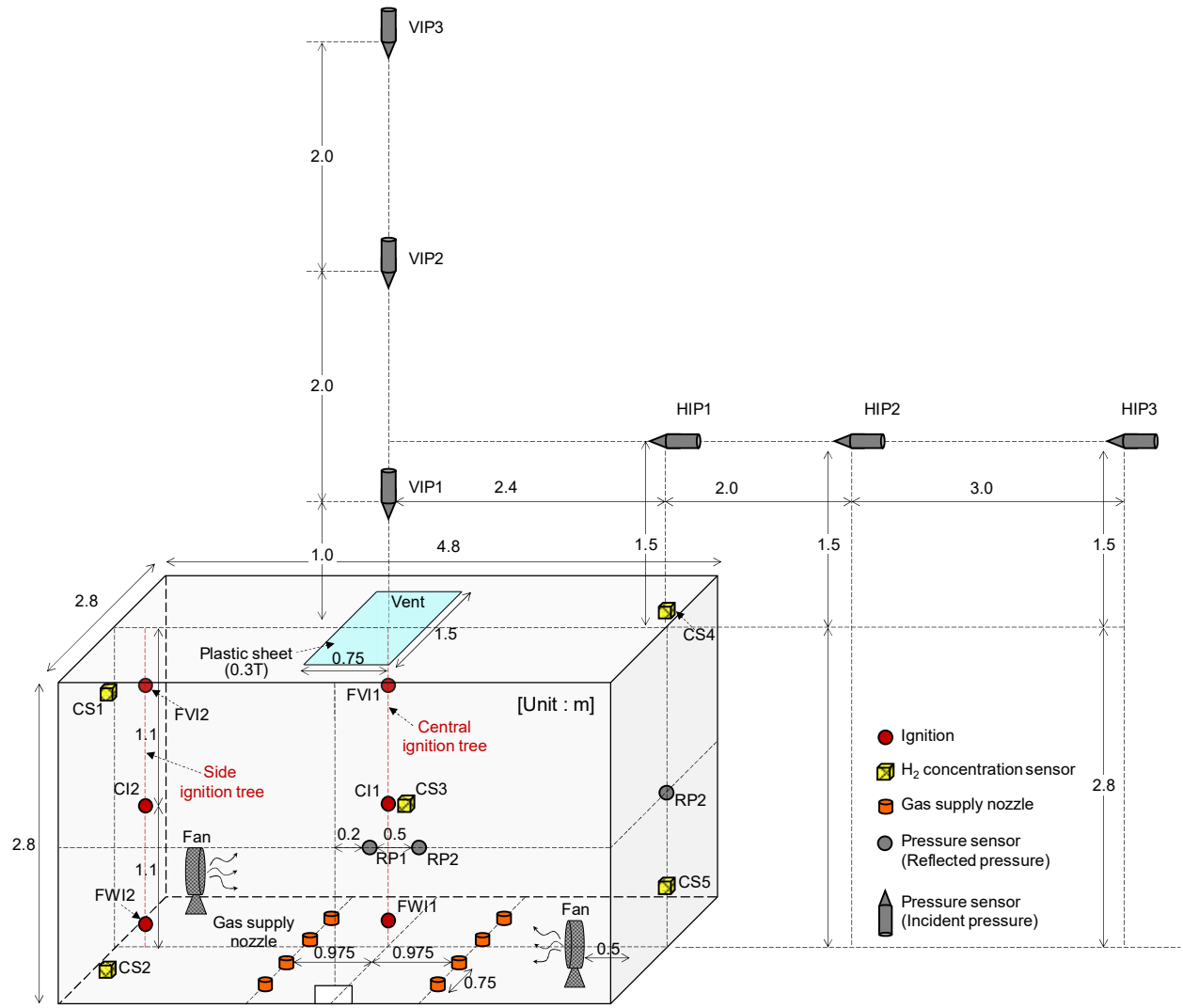
❖ This study conducted an experiment to identify the effect of vented deflagration depending on the ignition location in a concrete structure filled with hydrogen-air gas mixtures in the enclosure.



# 2. Methods and materials

## 2.1 Experimental structures and measuring instruments

Overview of experimental structure



Measurement related sensors and devices



## 2.2 Experiment conditions and method

### Experiment conditions

Test no.	Vent condition	Vent coefficient	Ignition location	Concentration of hydrogen	
1	$A_v = 1.13 \text{ m}^2$	$K_v = 6.62$	Central ignition tree	Front-vent ignition 1	29.0 %
2				Central ignition 1	
3				Floor-wall ignition 1	
4			Side ignition tree	Front-vent ignition 2	
5				Central ignition 2	
6				Floor-wall ignition 2	

### Vent condition

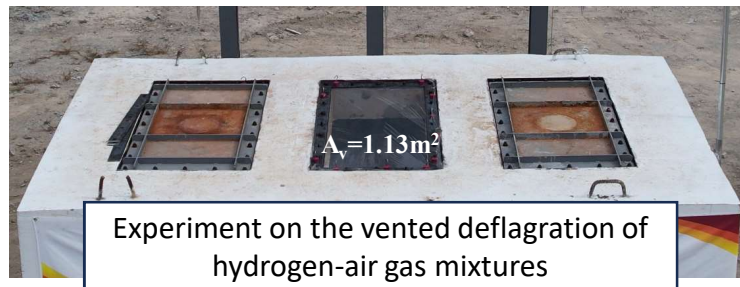
- NFPA 68 (2013) & KFS 720 (1998)

$$A_{v0} = A_s \frac{\left[ 1 - \left( \frac{P_{red} + 1}{P_{max} + 1} \right)^{1/\gamma b} \right]}{\left[ \left( \frac{P_{red} + 1}{P_{max} + 1} \right)^{1/\gamma b} - \delta \right]} \frac{S_u \rho_u \lambda}{G_u C_d}$$

Where  $A_{v0}$ – the vent area calculated,  $\text{m}^2$ ;  $A_s$ – the enclosure internal surface area,  $\text{m}^2$ ;  $P_{red}$ – the maximum pressure developed in a vented enclosure during a vented deflagration, bar-g;  $S_u$ – fundamental burning velocity of gas-air mixture, m/s;  $\rho_u$ – mass density of unburned gas-air mixture,  $\text{kg}/\text{m}^3$ ;  $\lambda$ – ratio of gas-air mixture burning velocity;  $G_u$ – unburned gas-air mixture sonic flow mass flux,  $\text{kg}/\text{m}^2\text{-s}$ ;  $C_d$ – vent flow discharge coefficient;  $P_{max}$ – the maximum pressure, bar-g;  $\gamma b$ – ratio enclosure pressure prior to ignition, bar-g.

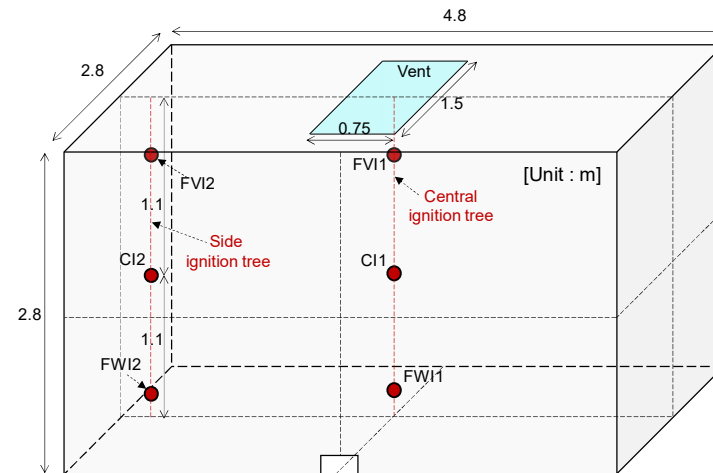
KFS720, 1998. Standard on venting of deflagrations code.

NFPA68, 2013. Standard on explosion protection by deflagration venting code.



### Ignition location conditions

- Central ignition tree (Front-vent ignition1, Central ignition1, Floor-wall ignition1)
- Side ignition tree (Front-vent ignition2, Central ignition2, Floor-wall ignition2)



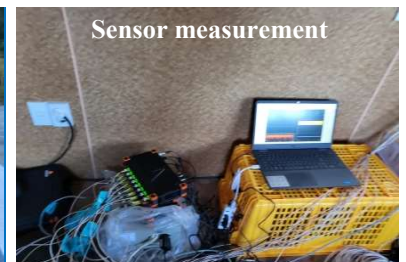
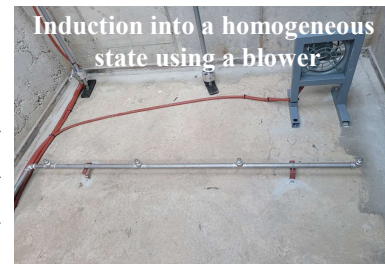
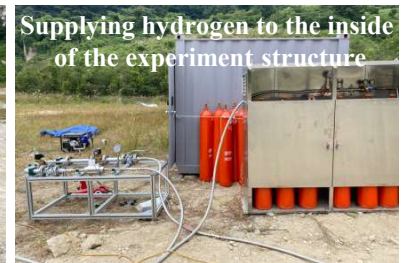
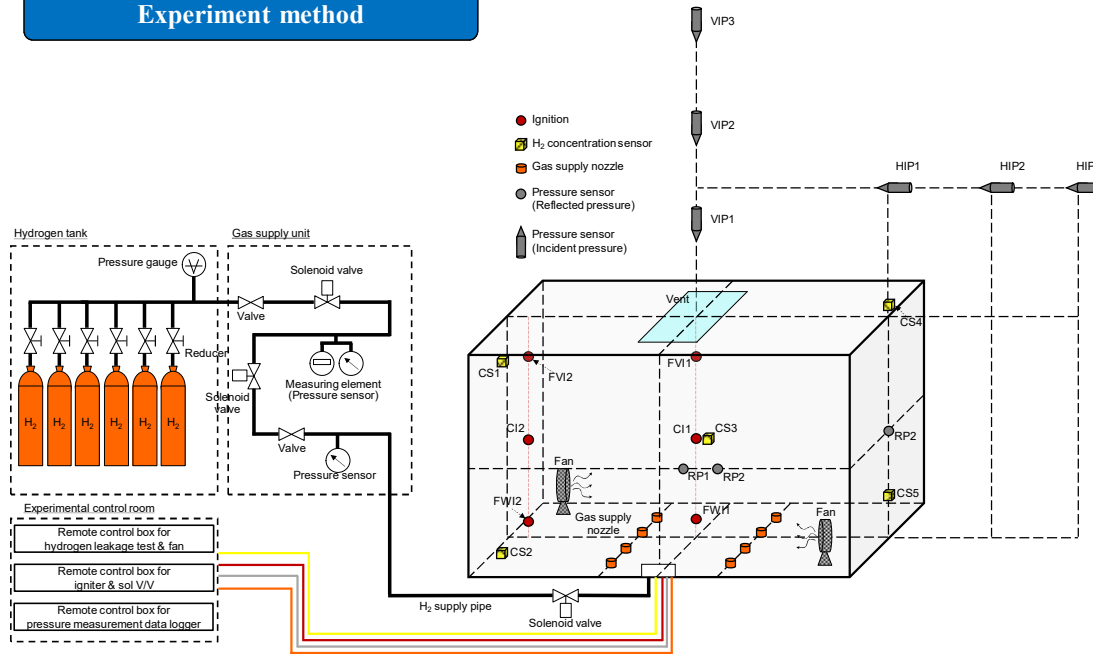
### Hydrogen concentration conditions

We set the hydrogen concentration at 29.0 %, corresponding to an equivalence ratio ( $\phi$ ) of 1.0, in which the hydrogen-air combustion reaction proceeds efficiently

# 2. Methods and materials

## 2.2 Experiment conditions and method

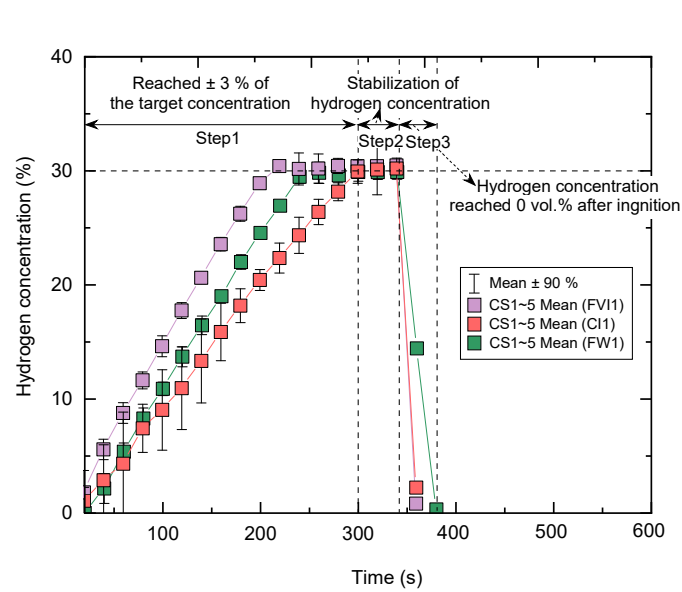
### Experiment method



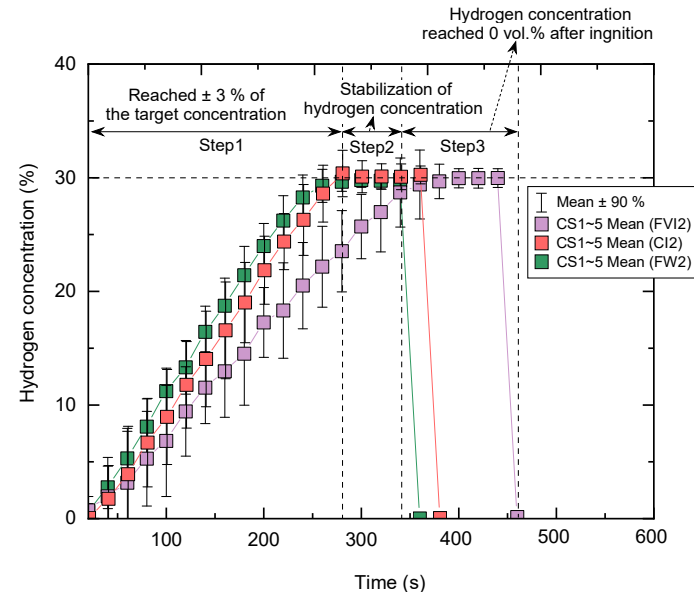
No.	Contents
1	Airtight condition using vinyl sheet
2	Supply hydrogen to the inside of the experiment structure
3	Stop supplying hydrogen when the hydrogen reaches $\pm 3\%$ of the desired range
4	Use a blower to induce good mixing of hydrogen and air in the space
5	When the hydrogen concentration in the space stabilizes, the data logger and thermal imaging camera are activated
6	Ignite the mixed gas; explosion occurs immediately after ignition
7	Measure the incident pressure and reflected pressure in units of time using a pressure sensor connected to the data logger

# 3. Results and discussion

## 3.1 Hydrogen concentration histories of the roof vented deflagrations

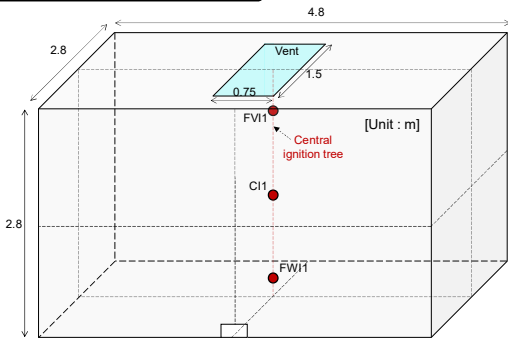


Central ignition tree

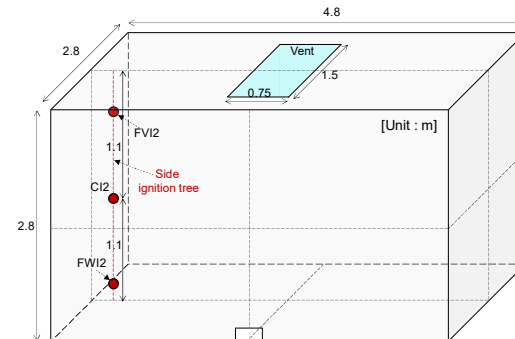


Side ignition tree

Ignition location conditions



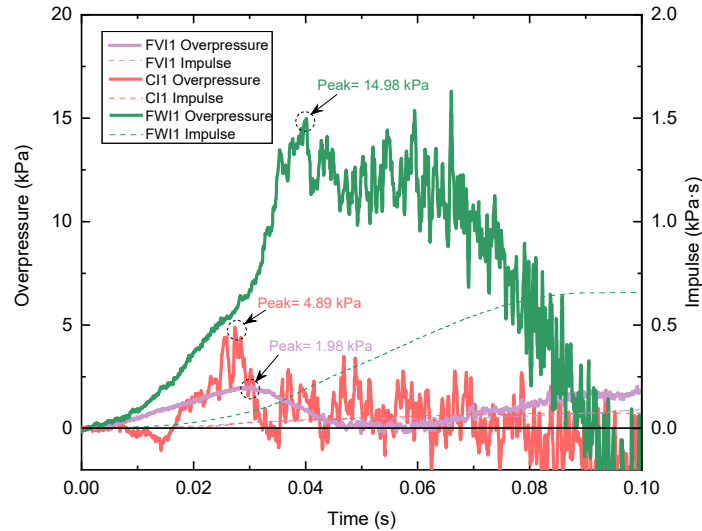
Central ignition tree  
(Front-vent ignition1, Central ignition1, Floor-wall ignition1)



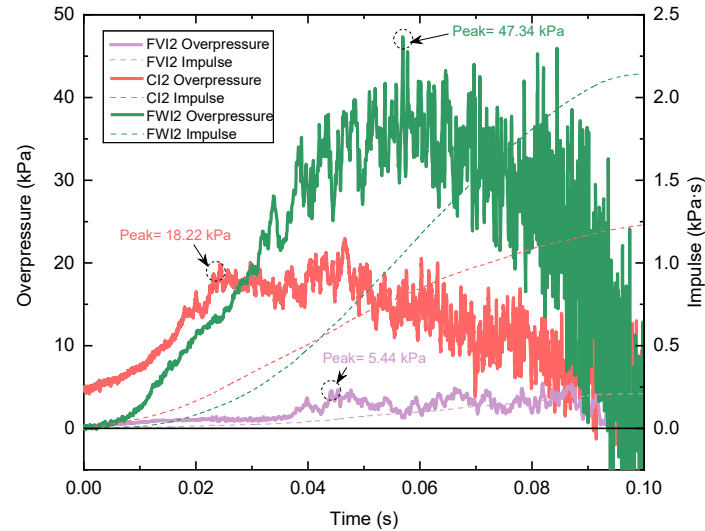
Side ignition tree  
(Front-vent ignition2, Central ignition2, Floor-wall ignition2)

# 3. Results and discussion

## 3.2 Overpressure recordings in roof vent deflagration (Reflected pressure, RP)

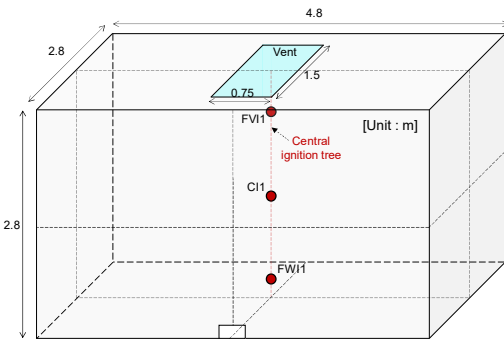


Central ignition tree

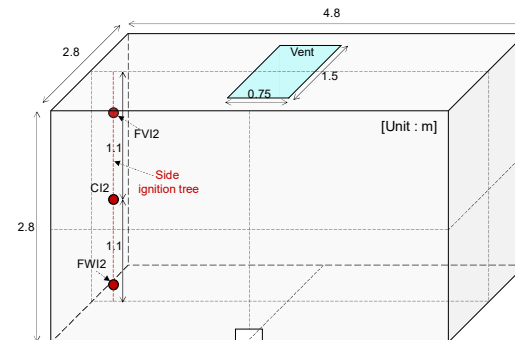


Side ignition tree

### Ignition location conditions



Central ignition tree  
(Front-vent ignition1, Central ignition1, Floor-wall ignition1)

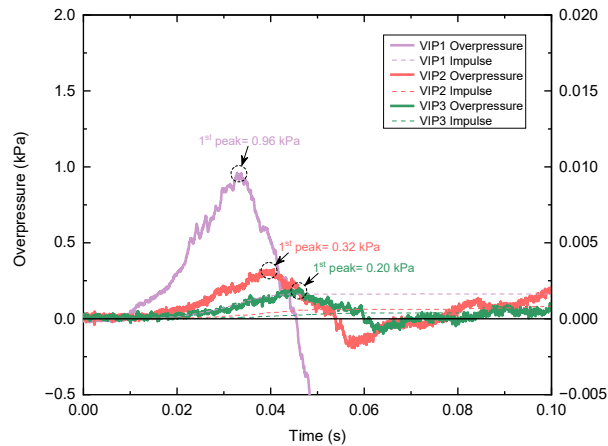


Side ignition tree  
(Front-vent ignition2, Central ignition2, Floor-wall ignition2)

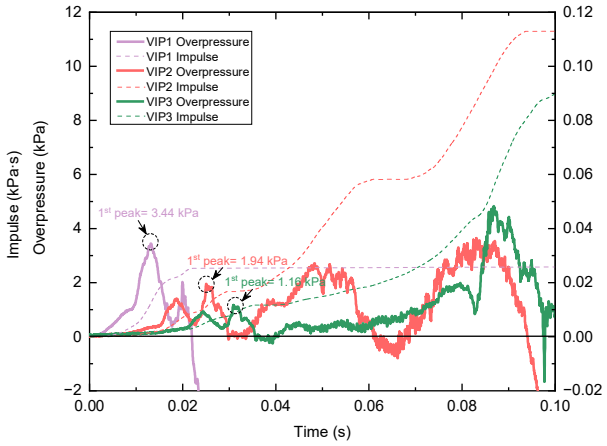
# 3. Results and discussion

## 3.2 Overpressure recordings in roof vent deflagration (Vertical incident pressure, VIP)

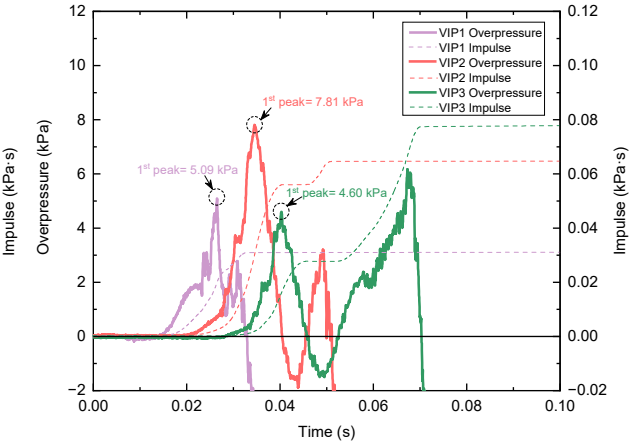
Central ignition tree



Front-vent ignition 1

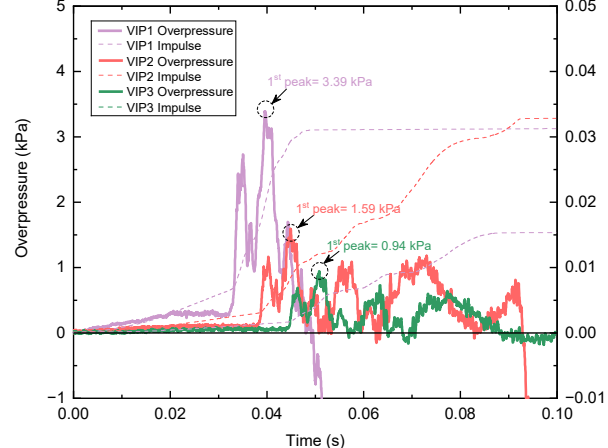


Center ignition 1

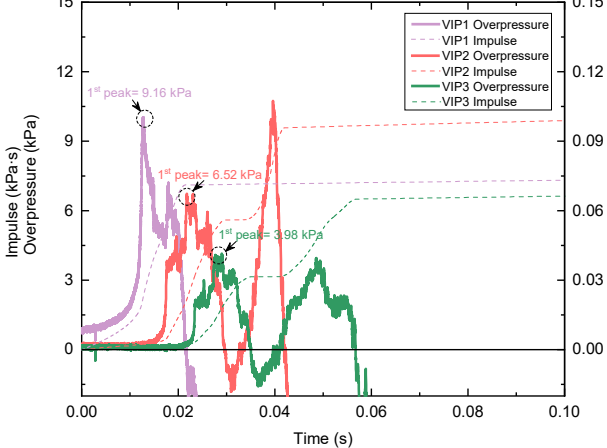


Floor-wall ignition 1

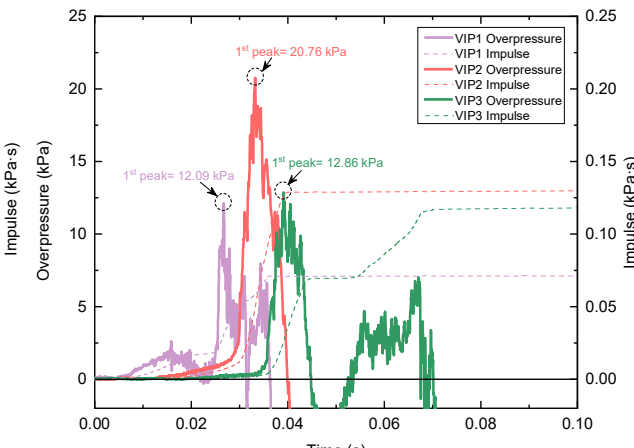
Side ignition tree



Front-vent ignition 2



Center ignition 2

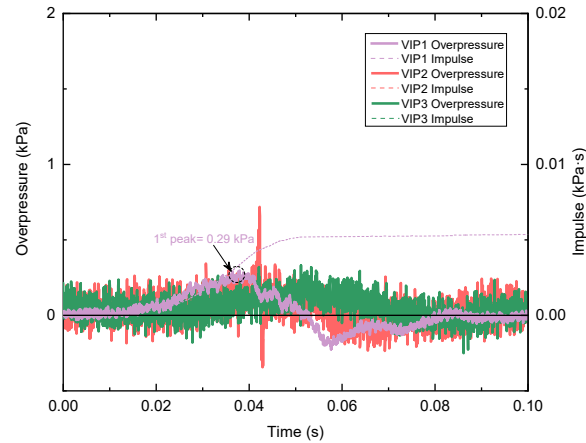


Floor-wall ignition 2

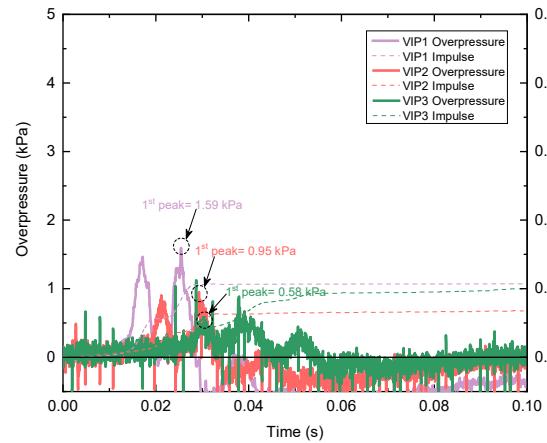
# 3. Results and discussion

## 3.2 Overpressure recordings in roof vent deflagration (Horizontal incident pressure, HIP)

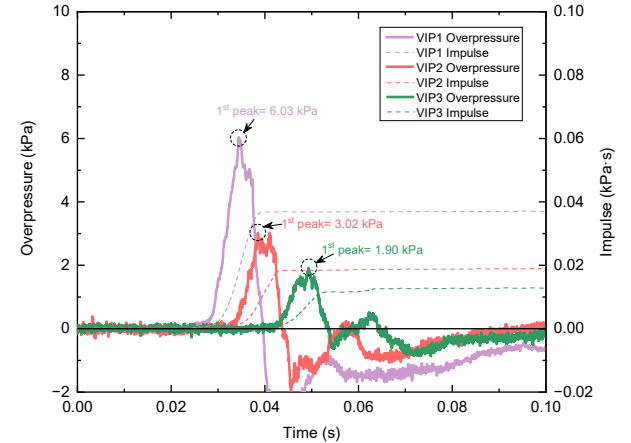
Central ignition tree



Front-vent ignition 1

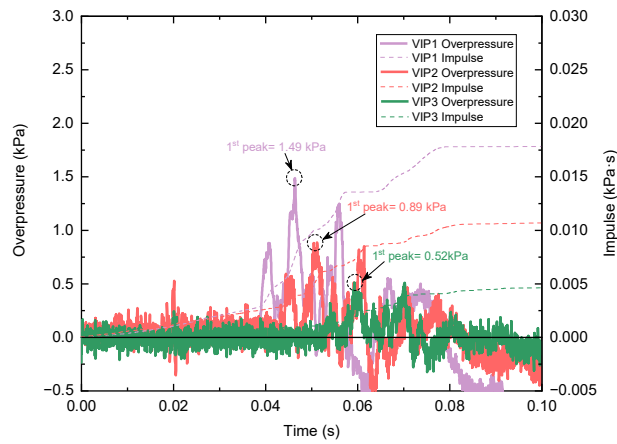


Center ignition 1

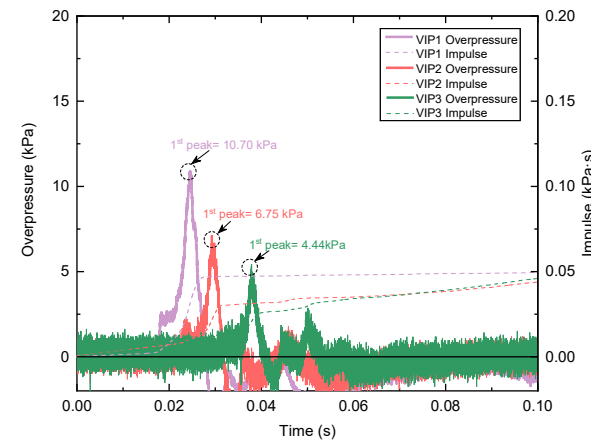


Floor-wall ignition 1

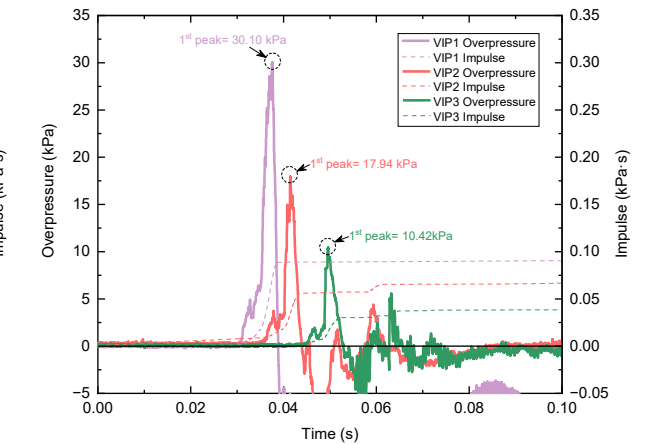
Side ignition tree



Front-vent ignition 2



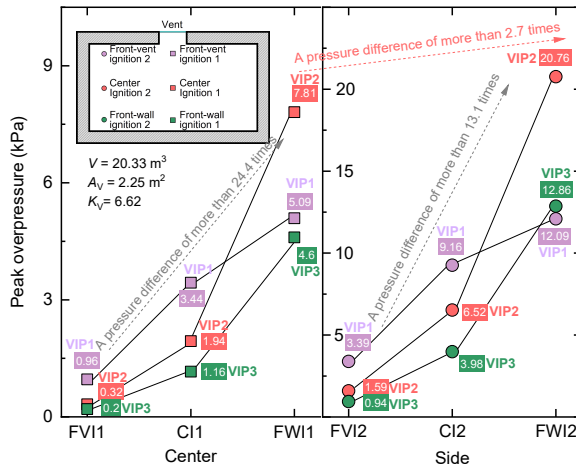
Center ignition 2



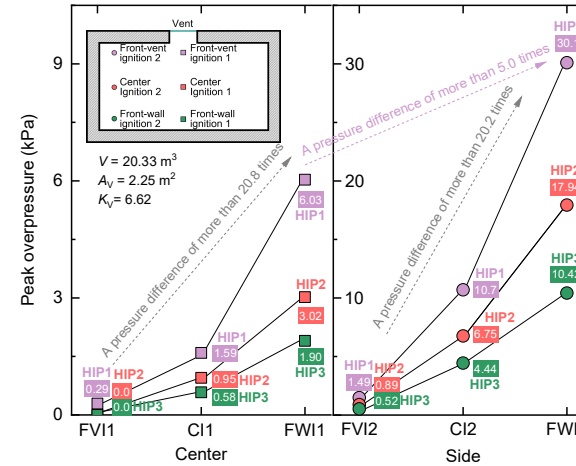
Floor-wall ignition 2

# 3. Results and discussion

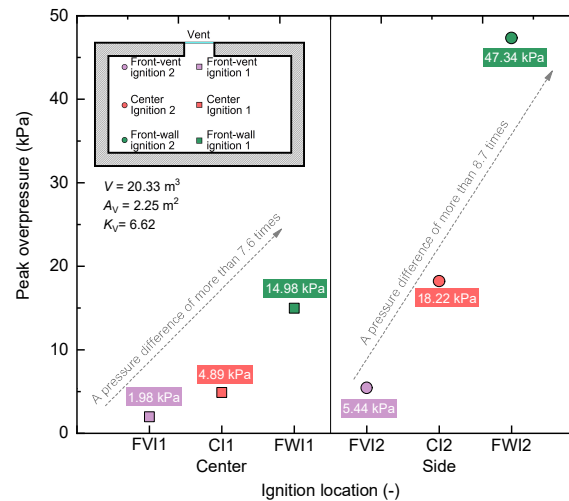
## 3.3 Effect of ignition location on peak overpressure value



Vertical incident pressure



Horizontal incident pressure

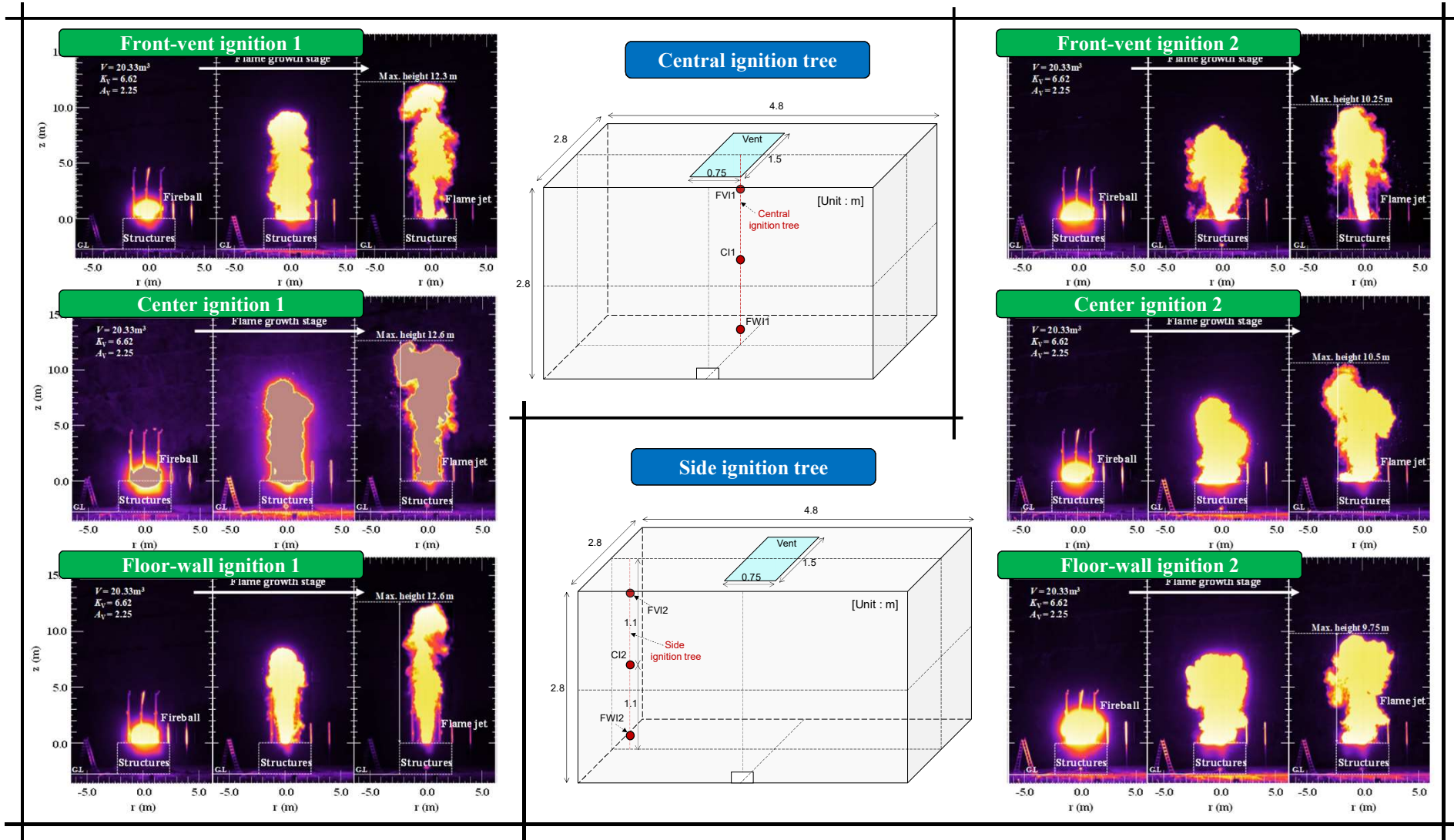


Reflected pressure



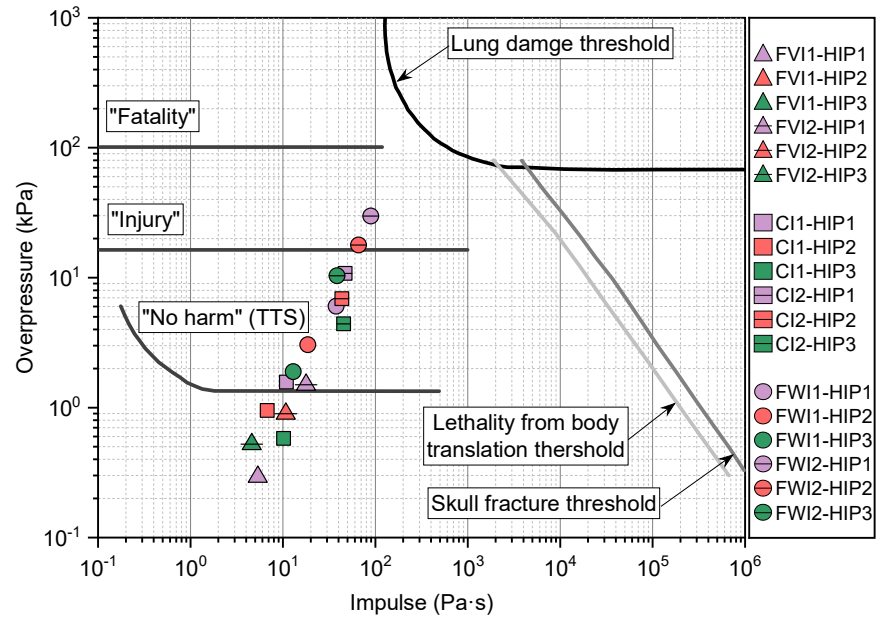
# 3. Results and discussion

## 3.4 Effect of ignition location on external flame behavior



## 3.5 Damaging effect on humans from vent explosions

Overpressure-impulse thresholds of harm criteria for humans



Effects of blast waves on human health

Incident pressure (kPa)	Damage level
13.8	Eardrum rupture threshold
16.5	1 % eardrum rupture probability
23	1 % eardrum rupture
25 ~ 35	1 % fatality probability
34.5 ~ 48.3	50 % eardrum rupture probability
35	15 % fatality probability
50 ~ 100	50 % fatality probability

## 4. Conclusions

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In this study, we conducted experiments to determine the effects of vent explosions according to the location of the ignition in a cuboid concrete structure (20.33 m<sup>3</sup>) with a vent (1.13 m<sup>2</sup>) on its roof, filled with a hydrogen-air mixture (29.0 Vol.%).

The main conclusions are summarized as follows.

**1**

With the increasing distance of the ignition source from the vent, the impact on overpressure and flame behavior increases, resulting in up to 24.4 times greater incident pressure values and up to 8.7 times greater reflected pressure values.

**2**

When exploring the behavior of the generated external flame, we observed that the shape of the formed flame differed according to the ignition location. In particular, the central ignition tree formed a flame with a long cylindrical column shape, whereas the side ignition tree formed a flame with a wide mushroom-cloud shape.

**3**

We predicted that distant ignition (FWI2, side ignition tree) might result in “Injury” level damage to humans (1% fatality probability) at a distance of 2.4 m away from the vent (HIP1), whereas almost no damage will occur at a distance of 7.4 m or more from the vent.

The results of this study are used as basic data for presenting design guidelines for explosion vents in underground spaces.

**Thank you for your attention !!**

**E-mail : [yoounggi@kict.re.kr](mailto:yoounggi@kict.re.kr)**

**Acknowledgments**

**This research was conducted under the KICT Research Program (project no. 20230104-001, Development of technology to secure safety and acceptability for infrastructure in hydrogen city) funded by the Ministry of Science and ICT**