

# Lab-scale dispersion of cryogenic hydrogen jets

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Presented at the PreSLHy Dissemination Conference

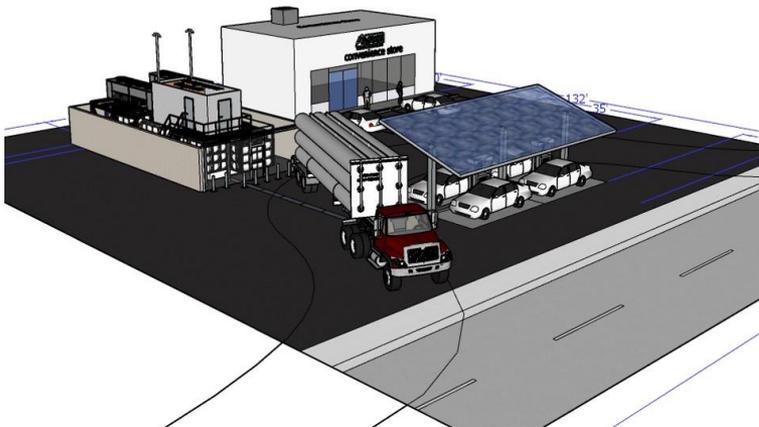
May 5, 2021

SAND2021-5510 C

# The objective of our work is to provide a scientific basis for exposure distances in the U.S. fire code, NFPA 2

## Compressed H<sub>2</sub> storage

- Previous work by Sandia led to science-based gaseous H<sub>2</sub> separation distances



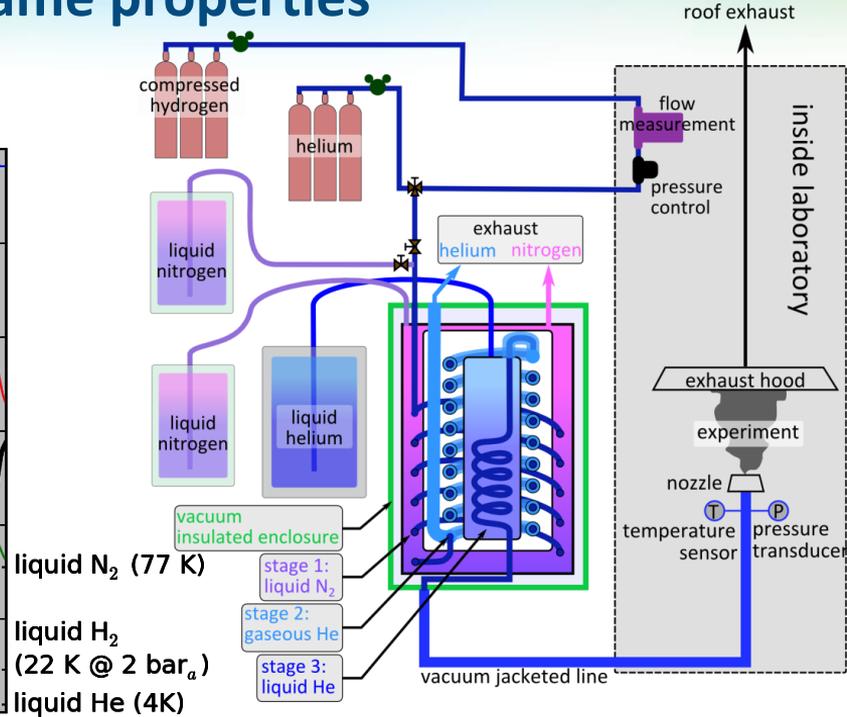
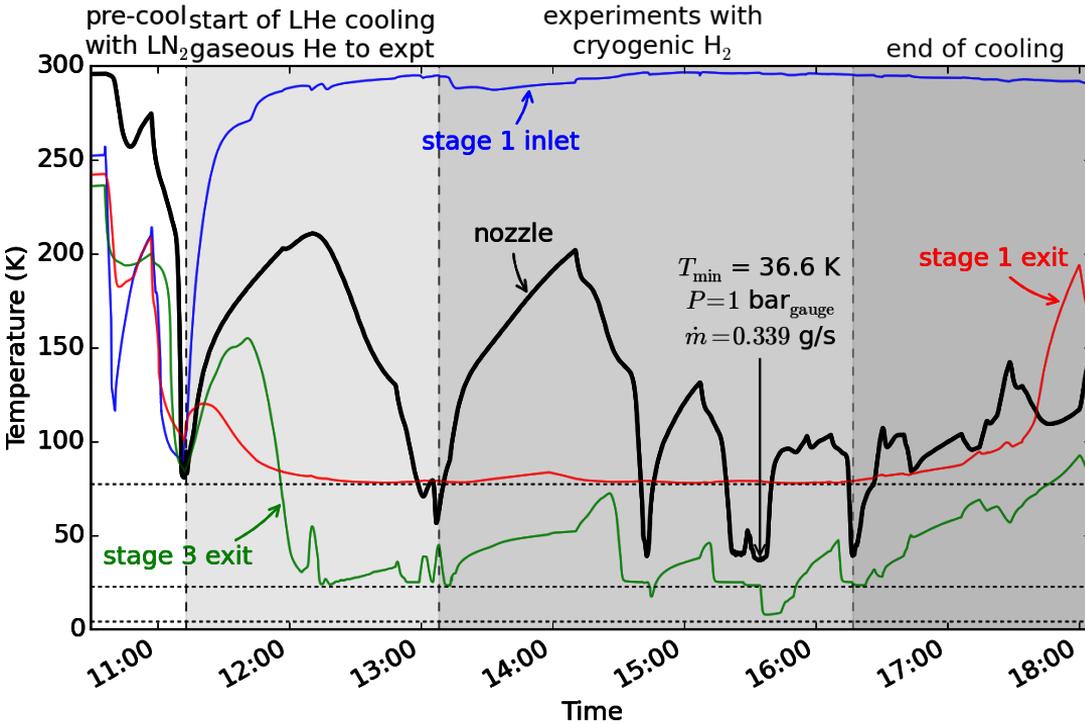
## Liquid H<sub>2</sub> storage

- Even with credits for insulation and fire-rated barrier wall, 75 ft. offset to building intakes and parking make footprint large

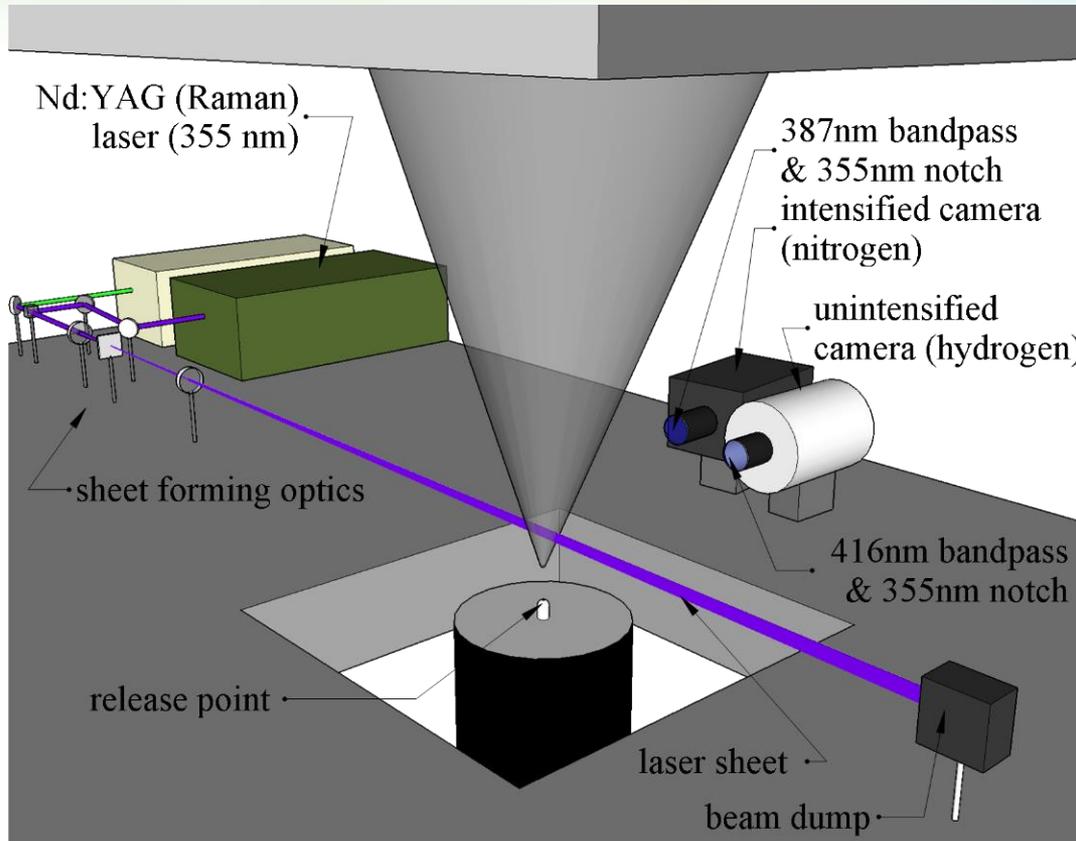


DOE goal: By September 30, 2022, identify ways to reduce the siting burdens that prohibit expansion of hydrogen fueling stations, through hydrogen research and development that enables a 40% reduction in station footprint, compared to the 2016 baseline of 18,000 square feet

# We have performed experiments releasing cryogenic hydrogen in the laboratory to study its dispersion and flame properties



# H<sub>2</sub>-N<sub>2</sub> Raman imaging has been used to measure concentration and temperature of cryogenic H<sub>2</sub>



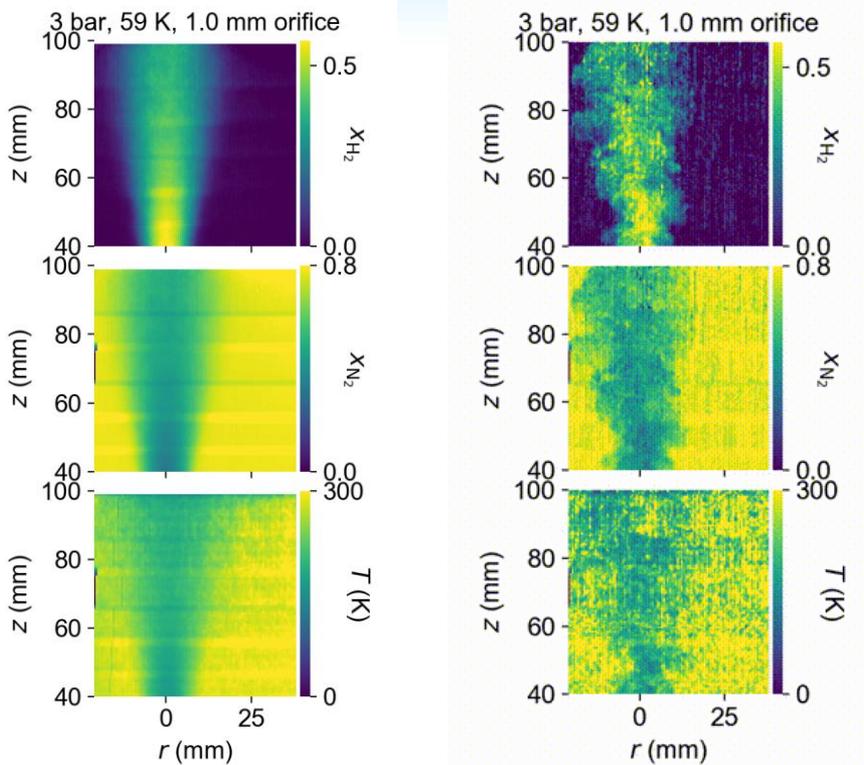
- Rayleigh used for room temperature releases, but signal overwhelmed by Mie scattering off of condensed water vapor in cryogenic jet
- Filtered Rayleigh had insufficient Mie scattering light suppression (OD $\approx$ 3)
- Raman scattering enables higher optical density filters
- Enables simultaneous measurement of concentration and temperature in 2D

# An experimental campaign with round nozzles had variations in temperature, pressure, and nozzle size

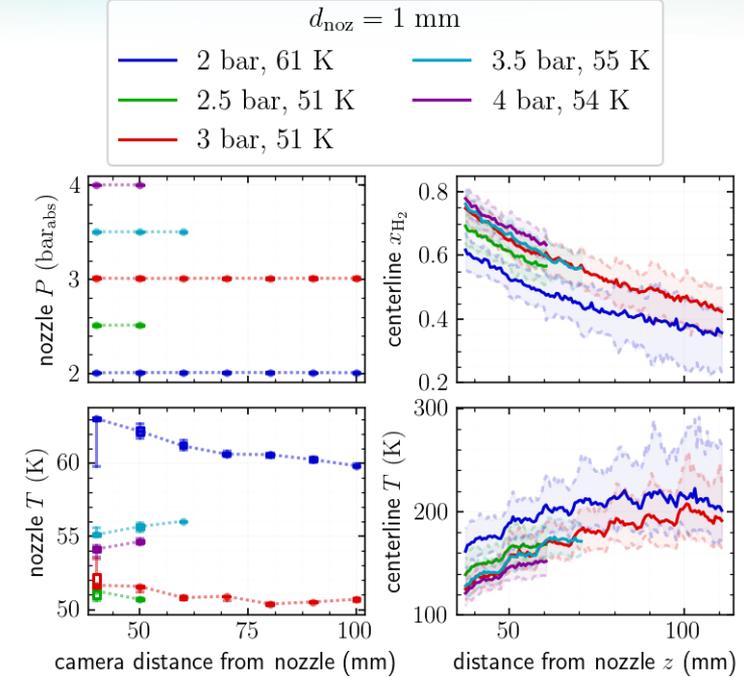
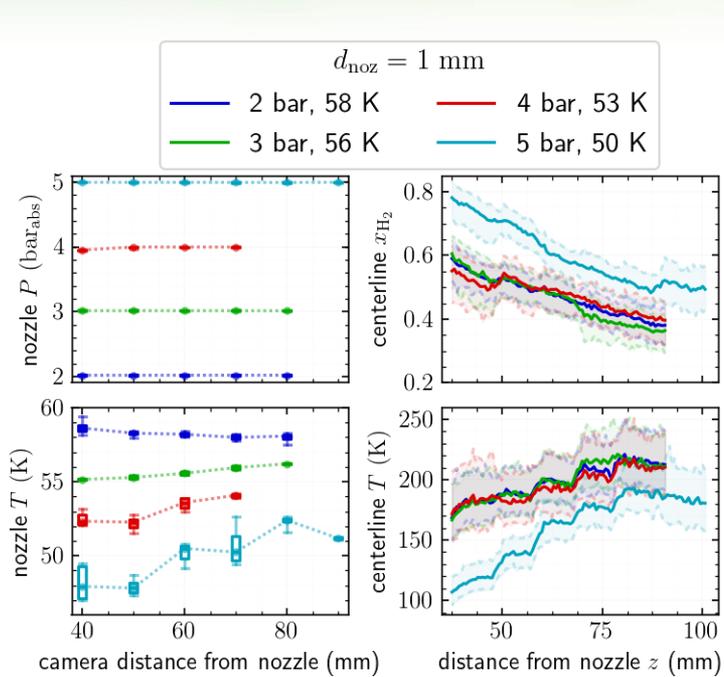
$T_{\text{noz}}$ [K]	$P_{\text{noz}}$ [bar <sub>abs</sub> ]	$d$ [mm]	$T_{\text{throat}}$ [K]	$n_{\text{ht}}$ <sub>s</sub>
58	2	1	43.5	4
56	3	1	41.9	4
53	4	1	39.6	4
50	5	1	37.4	5
61	2	1.25	45.7	6
51	2.5	1.25	38.2	2
51	3	1.25	38.2	6
55	3.5	1.25	41.2	3
54	4	1.25	40.4	2

Independent model parameters:

- ✓  $T$  - temperature
- ✓  $x$  - mole fraction
- ✓  $v$  - velocity
- ✓  $B$  - halfwidth (both velocity and concentration)

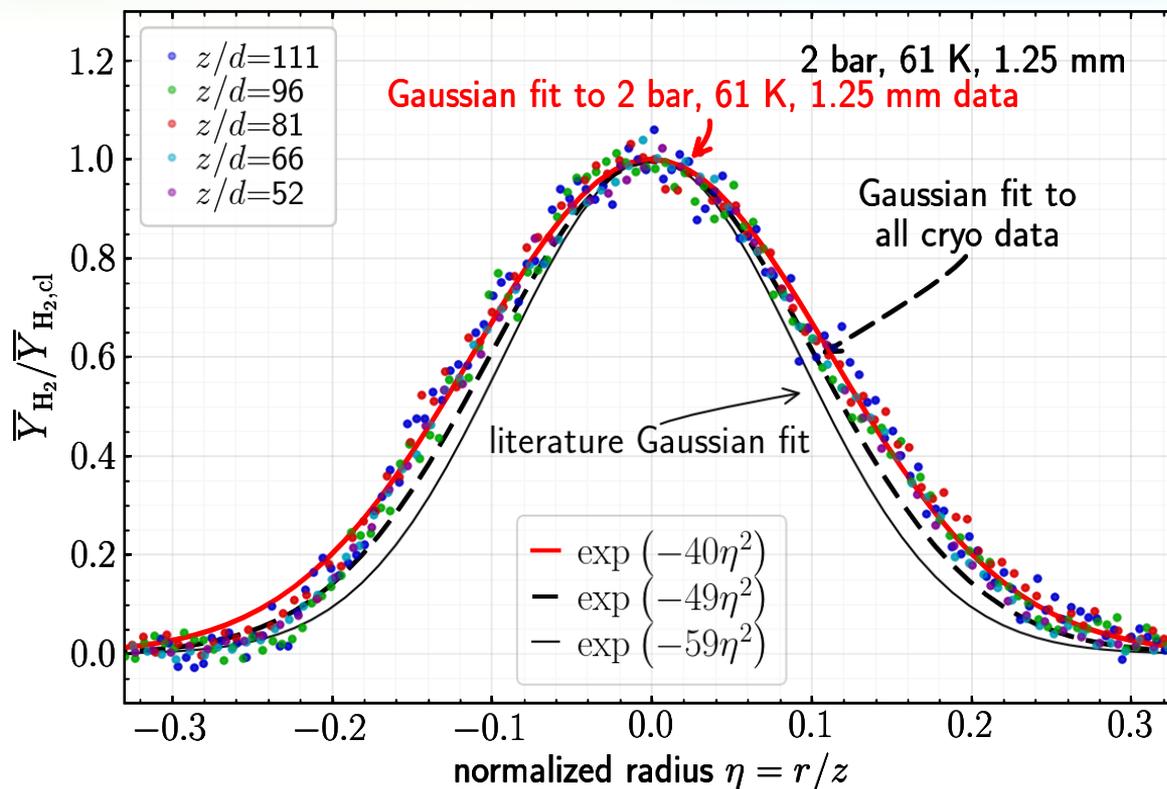


# Pressure at the nozzle was controlled; temperature was measured during experiments

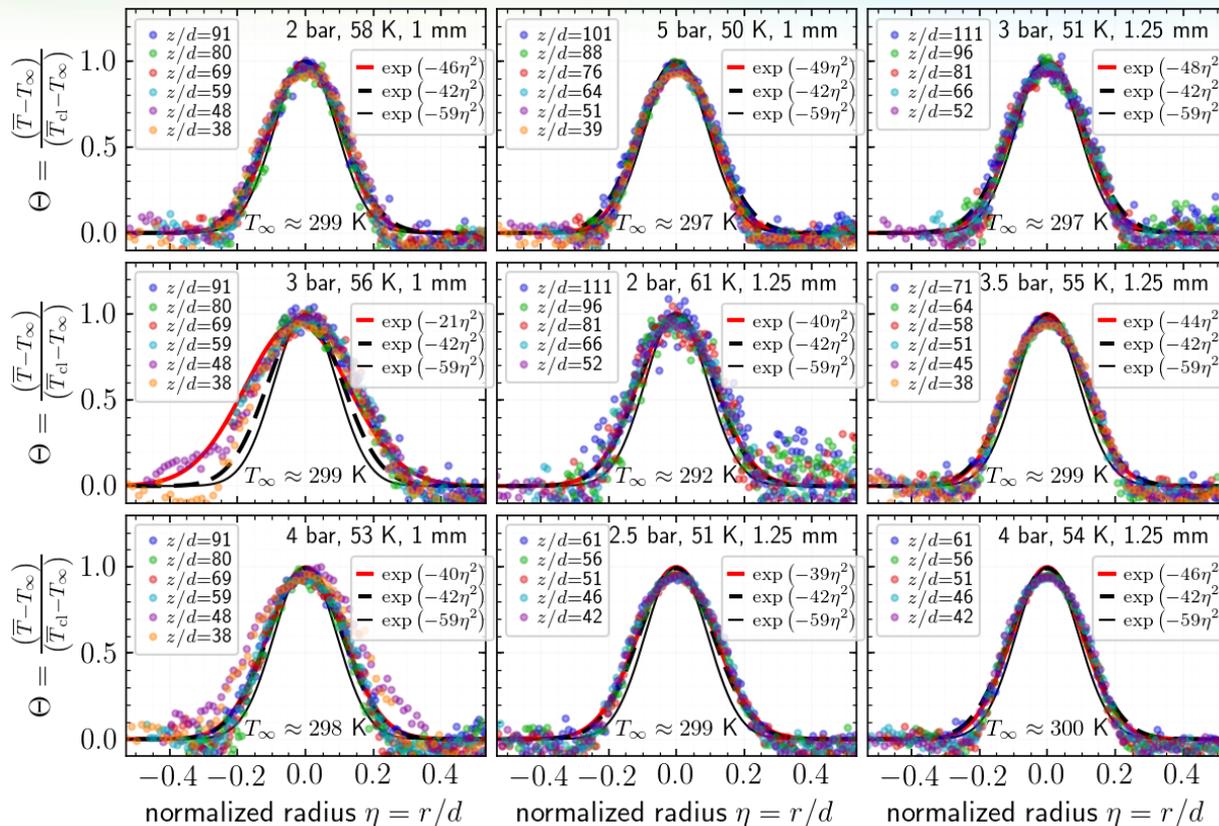


➤ Centerline mole fractions decrease and temperatures increase, as expected

# The 2-dimensional profiles are self-similar, and slightly wider than literature data of warm releases

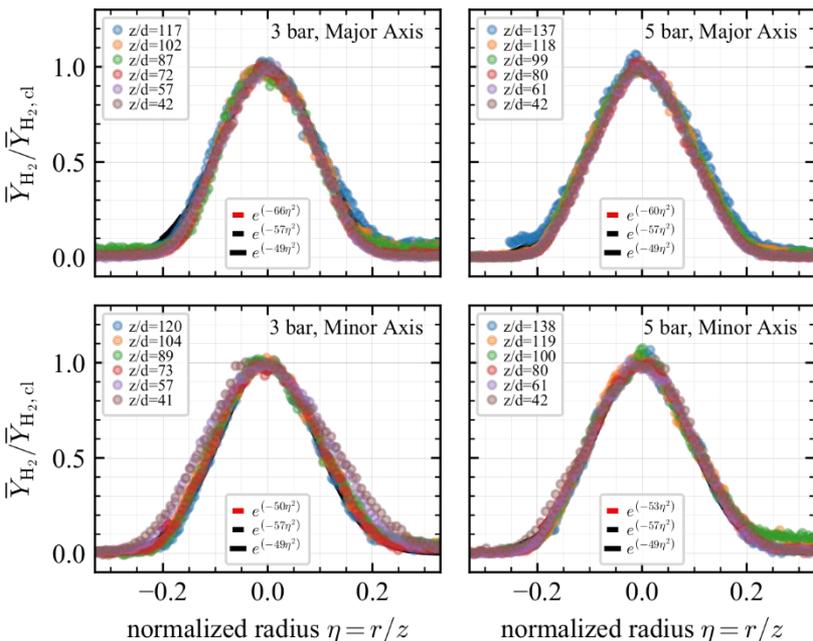


# Self-similar temperature fields were also measured

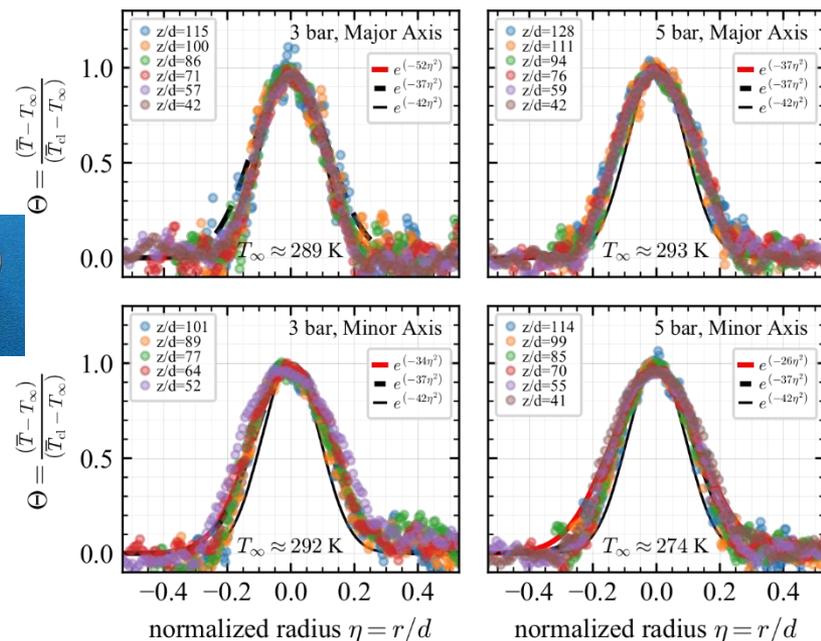


# Real leaks will likely not be round, so an experimental campaign was completed with high aspect ratio nozzles

Aspect ratio 32

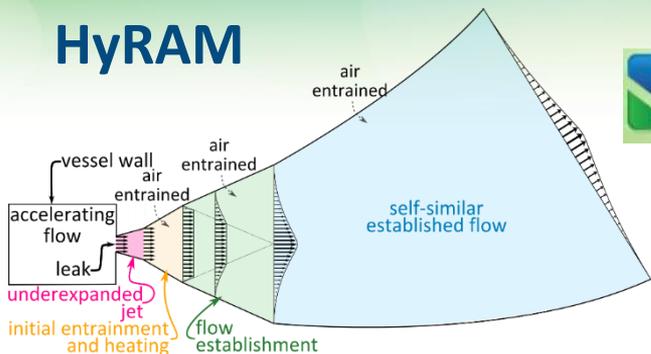


Aspect ratio 32

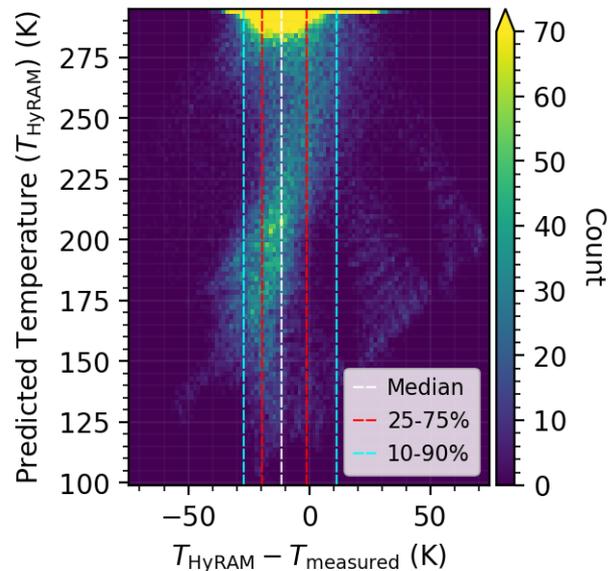
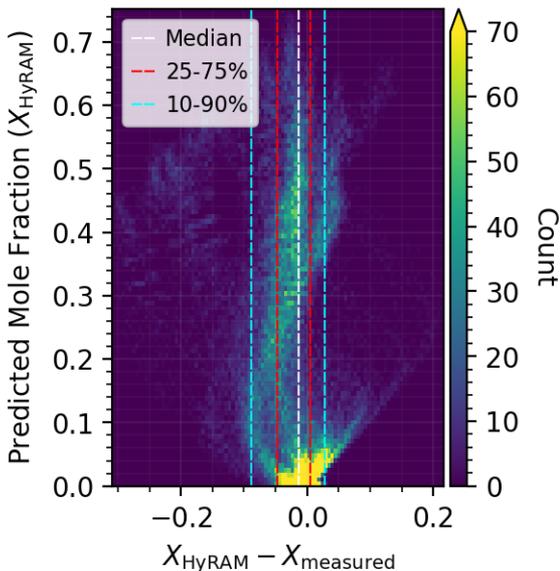
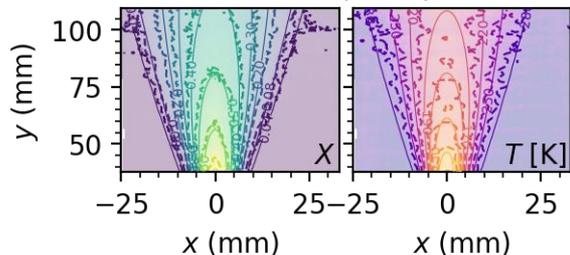


➤ No significant difference were observed (self-similar, Gaussian profiles) between high aspect-ratio nozzles and round nozzle profiles

# We have used lab-scale data to validate the dispersion model in HyRAM



$d = 1.25\text{mm}$ , 3bar, 51K



➤ Mole fraction and temperature predictions slightly lower than those measured but reasonably accurate

## Summary and conclusions on lab-scale dispersion

- Used advanced imaging diagnostics (planar laser Raman imaging) to measure cryogenic hydrogen mixing with air and warming
- Centerline mass fraction decay rate for cryogenic hydrogen similar to warm hydrogen
- Centerline temperature also increases linearly against normalized distance
- Mass-fraction (and temperature) profiles are self-similar, Gaussian, and slightly wider than for ambient temperature hydrogen
- Concentration and temperature fields of dispersion from AR 16 and 32 nozzles is the same as for round nozzles under these conditions (1 mm equivalent diameter,  $\approx 55$  K, 3 and 5 bar<sub>abs</sub>)
- Simulations using dispersion model in HyRAM are accurate, for round or even for high aspect-ratio release geometries
- Data from experiments is available upon request (*SAND2019-2199 O*, *SAND2020-3950 O*)



**QUESTIONS**

**COMMENTS**

**DISCUSSION**



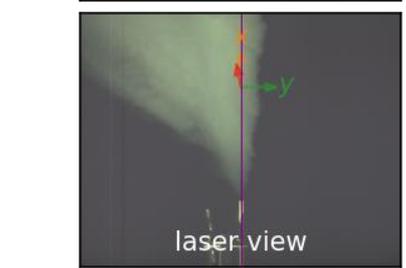
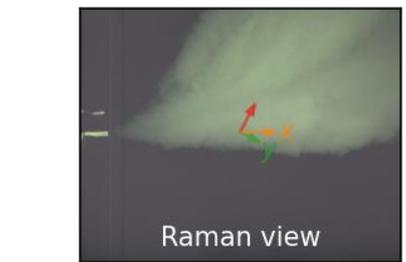
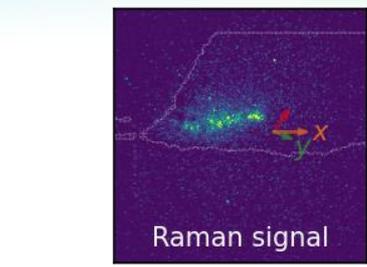
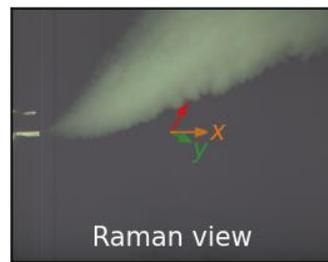
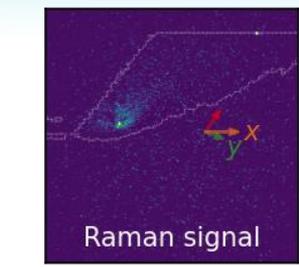
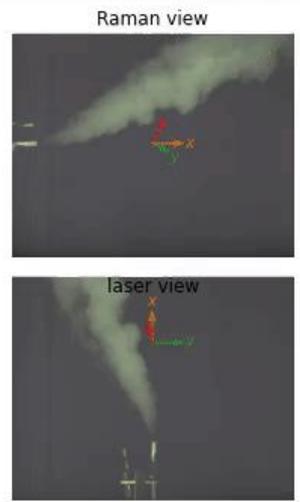
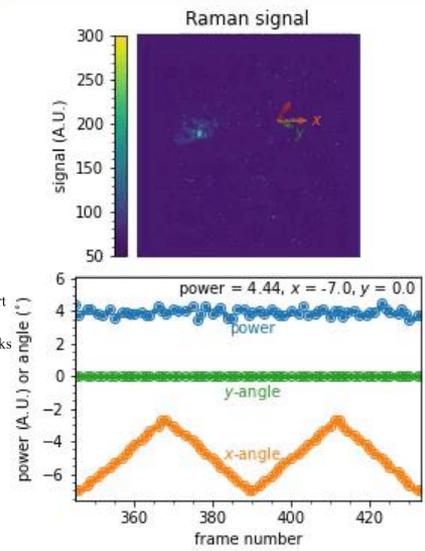
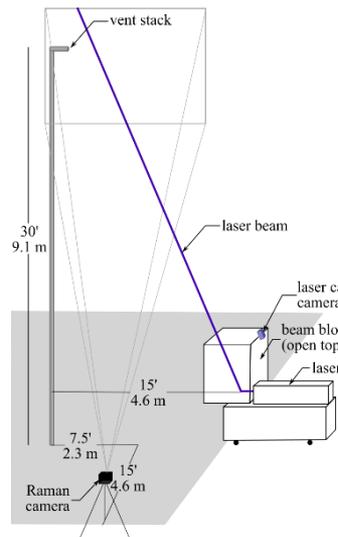
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Thanks for funding support from:

- United States Department of Energy, Energy Efficiency & Renewable Energy, Fuel Cell Technologies Office, Safety, Codes, and Standards subprogram managed by Laura Hill
- Industry support including the OEM Group at the California Fuel Cell Partnership, Linde, and Shell
- Air Liquide and partners

# More recently, we have demonstrated use of the Raman diagnostic for larger releases

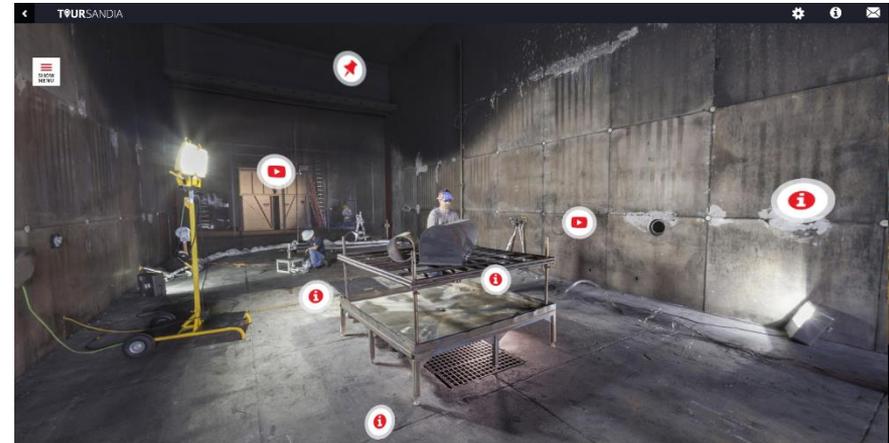
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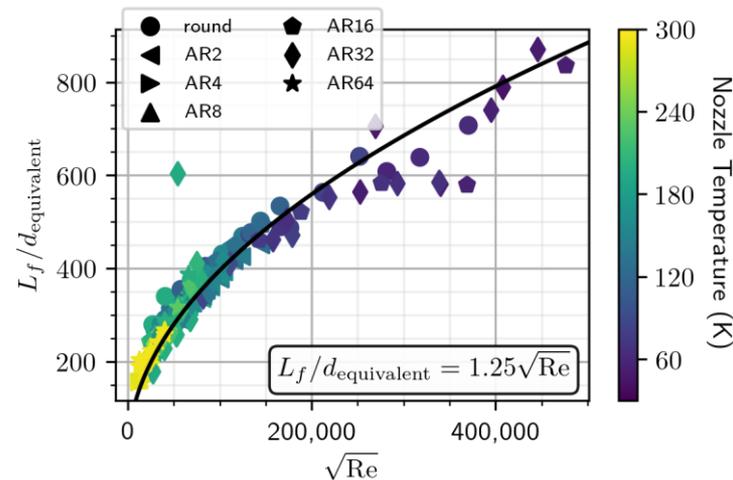
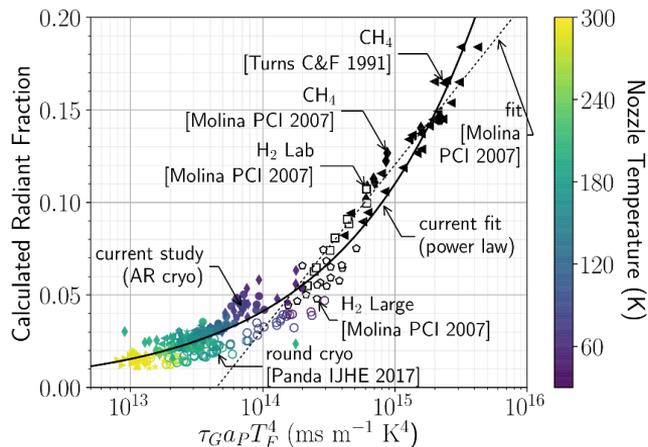
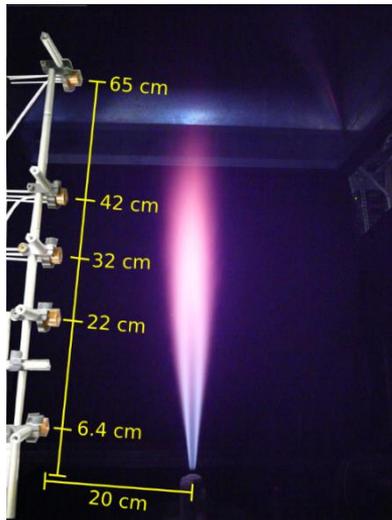
➤ As wind blows the visible plume off, then back on of the laser-line, the Raman signal disappears, then increases

# We are planning additional experiments to understand other phenomena related to liquid hydrogen

- Additional experiments are needed to address additional phenomena:
  - Controlled experiments at Sandia’s Cross-Wind Test Facility to validate models for:
    - Pooling
    - Evaporation from LH<sub>2</sub> pools
  - Revisit mitigation from walls, including dispersion and mitigation of liquid hydrogen leaks/flames
    - Effects on unignited dispersion and accumulation
    - Reduction in heat flux/overpressure
  - Partner with others, applying diagnostic at remote locations (European colleagues, CGA G-5.5 testing task force) and analyze external data



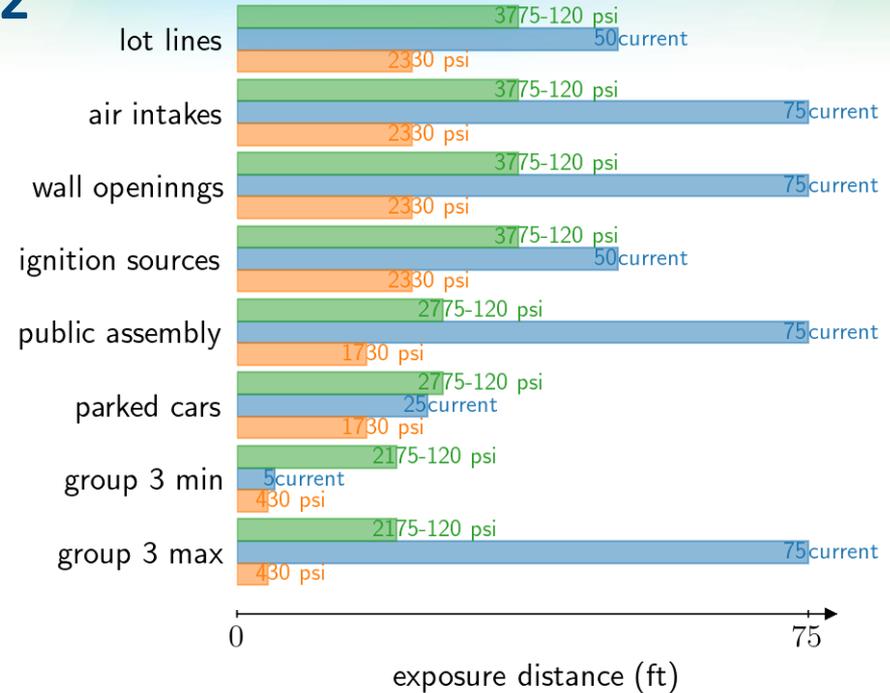
# Lab-scale experiments on flames from round and high aspect ratio nozzles have been used for model validation



- No clear aspect-ratio dependence for radiant fraction or flame length
- All data collapses onto a single curve for warm and cryogenic temperatures

# We have used HyRAM models to propose new liquid hydrogen exposure distance tables for NFPA 2

- Proposal submitted to first draft of NFPA 2
- Providing additional justification for subsequent revisions to code
- Separation distances grouped same as gaseous distances
- Distances function of pipe size and system pressure instead of tank volume
- Safety factor of 2 included to account for uncertainty (safety factor of 1.5 used for gaseous distances)



➤ Most distances reduced for typical pipe size (1.5") and operating pressure (vs typical tank volume); some increase (but mitigations, i.e. walls can be used)